FLOOR DISTRIBUTION OF STANDARD AUTOMATIC SPRINKLER HEADS

L. A. FOSCHINBAUR J. S. KULA R. F. SCHREINER

ARMOUR INSTITUTE OF TECHNOLOGY
1917

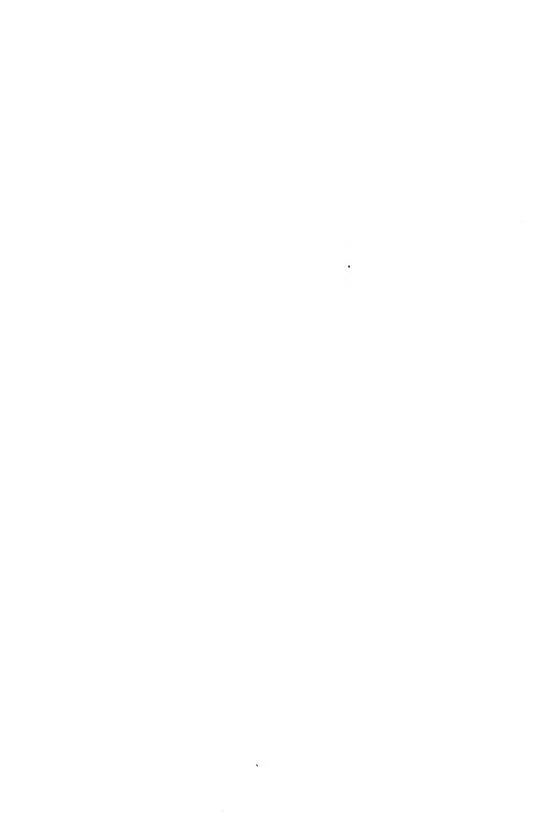
614.844 K 95



Minion Promittee
of Committees
UNIVERSITY Associations

AT 456
Kula, J. S.
Floor distribution of standard automatic

Digitized by the Internet Archive in 2009 with funding from CARLI: Consortium of Academic and Research Libraries in Illinois



			•	
	. 20			

FLOOR DISTRIBUTION OF STANDARD AUTOMATIC SPRINKLER HEADS

A THESIS

PRESENTED BY

J. S. Kula, L. A. Foschinbaur and R. F. Schreiner

TO THE

PRESIDENT AND FACULTY

OF

ARMOUR INSTITUTE OF TECHNOLOGY

FOR THE DEGREE OF

BACHELOR OF SCIENCE
IN

FIRE PROTECTION ENGINEERING

MAY 31, 1917

APPROVED:

ILLINOIS INSTITUTE OF TECHNOLOGY PAUL V. GALVIN LIBRARY 35 WEST 33RD STREET CHICAGO, IL 60616 Professor of Fire Protection Engineering

Dean of Engineering Studies

Dean of Cultural Studies



PREFACE.

The object of this investigation was to study the floor distribution of standard automatic sprinklers. The work was of a similar nature to that performed in the past two years by Senior students in the Fire Protection Engineering course of Armour Institute of Technology. This investigation will probably be continued with the ultimate object, by means of sufficiently thorough and exhaustive tests, and by the curves drawn and data compiled, of drawing up standard specifications for the "Floor Distribution of Standard Automatic Sprinklers" for Underwriters Laboratories.

The authors wish to take this opportunity of expressing their sincerest thanks to Mr. H. H. Allport, Assistant Professor of Fire Protection Engineering at Armour Institute of Technology, and to Mr. J. E. Evans, of

, in the second of the second

· •

*

the Sprinkler Department of Underwriters Laboratories, for their cooperation in this investigation.

L. A. Foschinbaur

J. S. Kula

R. F. Schreiner.

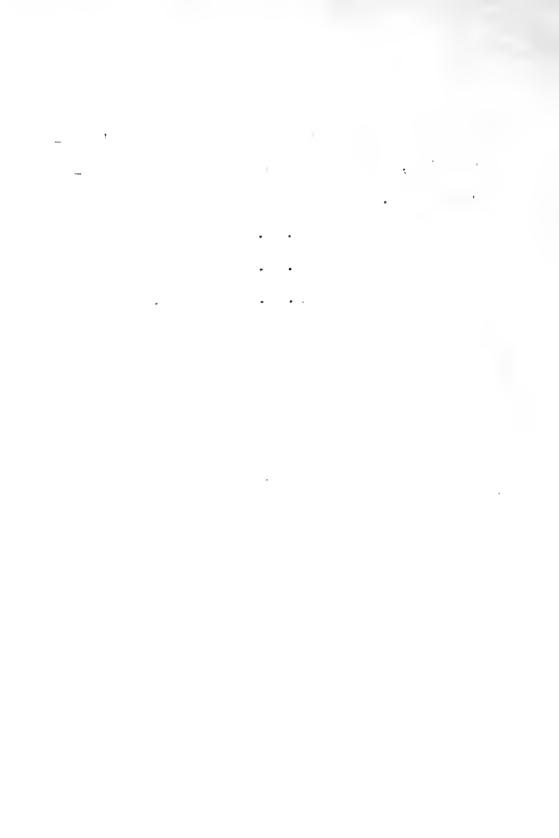


TABLE OF CONTENTS	D
Title Page	Page
Preface	
Introduction	
List of Illustrations	
PART ONE - DISCHARGE	
Apparatus	2
Test Method	3
Discussion and Results	5
PART TWO - DISTRIBUTION	
Apparatus	14
Test Method	16
Discussion and Results	19
PART THREE - CONCLUSION	
Conclusions	22
Data and Diagrams	3/

INTRODUCTORY.

The investigation of the Floor Distribution of Standard Automatic Sprinklers was carried in two distinct sections, namely, Discharge and Distribution and will be discussed under three heads.

Part 1. Discharge

Part 2. Distribution

Part 3. Conclusions.

A brief outline of the object of each section will be given here, while a detailed account of the methods of test will be treated separately.

The object of Part 1 is to secure a curve, by means of which, knowing the pressure in pounds per square inch on an automatic sprinkler head in operation, the discharge in gallons per minute may be directly read.

The object of Part 2 is (a) to secure a "zone distribution" curve, showing the distribution over each "zone" in gallons per square foot per minute and (b) to secure a "sector



distribution" curve showing the distribution over each "sector" in per cent of the theoretical amount of water in each sector.

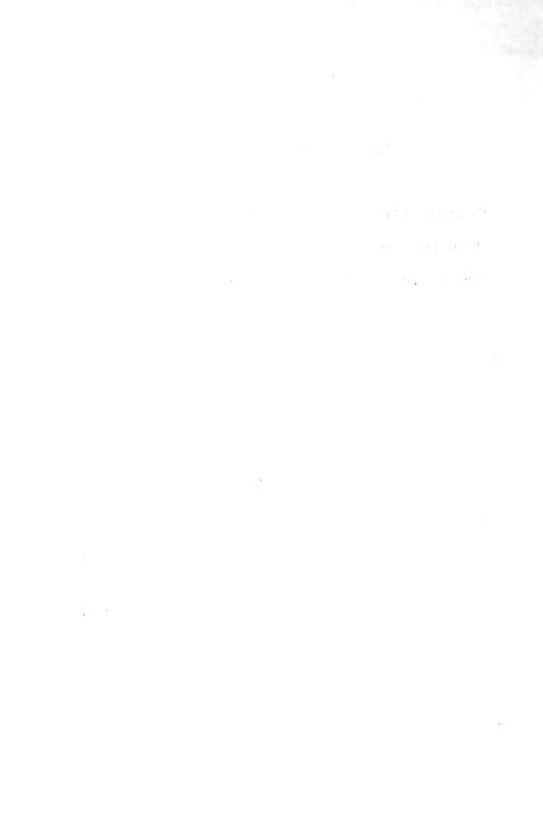
The object of Part 3 is to draw conclusions, by means of the curves secured in Part 2,
as to the pressure and distance of head from
ceiling that will give the most satisfactory
floor distribution.

Later on, when a sufficient number of heads have been tested, general conclusions can be drawn and specifications drawn up, as to what shall constitute a satisfactory floor distanction.



LIST OF ILLUSTRATIONS

	Page
General View of Apparatus	28
Pans Uncovered	29
Cross Sectional View of Heads	30



Part <u>1</u>

DISCHARGE.



a) Apparatus --

The apparatus used consisted of the follow-ing:

A cylindrical tank of four feet diameter with a capacity of two hundred and fifty gallons. The contents of the tank was read by means of an ordinary gauge glass, calibrated to read to tenths of a gallon. The tank could be emptied by means of a quick opening outlet valve at the bottom.

The sprinkler head to be tested was installed in the piping as shown in Fig.1, with the addition of a length of pipe three feet long, fastened to the swivel pipe, so that the whole arrangement could be swung around from one position to another. At the end of this length of pipe, the piezometer connection was made and from this connection, a rubber patrol hose lead to the two gauges, one reading from zero to fifty pounds and the other reading from zero to two hundred pounds, and used respectively for pressures from zero to twenty-five



pounds up. (See Fig. 1)

The pressure was regulated by means of a valve, operated by a long stem and a hand wheel. The water supply was received from a Quimby Fire Pump, pumped over to a forty-five hundred gallon vertical pressure tank.

The flexibility of pressure desired was secured by means of an air cushion in the pressure tank, the supply of air being received from an air compressor.

The heads used were 165 degree heads of the following makes:

The Esty, the Niagara and the Manufacturerers.

b) - Test Method .

The head was installed in the piping and the tank placed in position so that the head was directly over the center of the tank. On the end of the pipe, placed over the sprinkler head was an inverted galvanized iron cylindrical hood, to direct all the discharged water into the tank. The tank was made perfectly level, so that there would be no errors in the reading of the gauge glass.



The pipe was then swung away from the tank by means of a large pole, to a sufficient distance to prevent water splashing over into the tank when the pressure was turned on.

The pressure was then adjusted to a definite value, by means of the long stemmed valve, after the zere point of the gauge glass had been read, and, at a given signal, the head was swung back over the center of the tank. A five or seven minute run was made, during which time the pressure was kept constant. At the expiration of the time the head was swung away from the tank and the pressure turned off. After the surging in the tank had subsided, the gauge glass reading was taken.

Pressures were taken at five pound intervals from sixty pounds per square inch down to ten pounds per square inch and from there down to three pounds per square inch at one pound intervals.



DISCUSSIONS AND RESULTS.

From the data obtained, pressure discharge curves were plotted. The pressure in pounds per square inch was plotted as abcissae and the discharge in gallons per minute was plotted as ordinates. From the resulting curves, it is possible to find the discharge if the pressure is known, and vice versa, for each head.

By studying the general shape of the curves it is seen that they resemble each other to some extent and theoretically they should, because, if the formula, which shows that the velocity is caused by a certain static head, is analysed, it is seen that the equation is of the second degree and therefore when plotted on coordinate paper, the resulting curve is a parabola. For this reason all the pressure-discharge curves resemble parabolas.



If an equation of the second degree is plotted on logarithm paper a straight line will be obtained. If the data obtained in these tests are plotted on logarithm paper a straight line will be obtained for one part of the test and another straight line for the second part of the test. These lines will intersect. if extended. This fact indicates then, that the pressure discharge, is really made up of two parabolas. These two parabolas have slightly different slopes because the constant in the equation changes slightly in the latter part of the test.

discharge curve is made, it is seen that for pressures up to about 40# per square inch, the Manufacturers head has the greatest discharge, the Esty and Niagara heads having a lower and most identical discharge. As the pressures go above 40# per square inch the discharges from each head are almost equal.

•

_ .

· ·

•

•

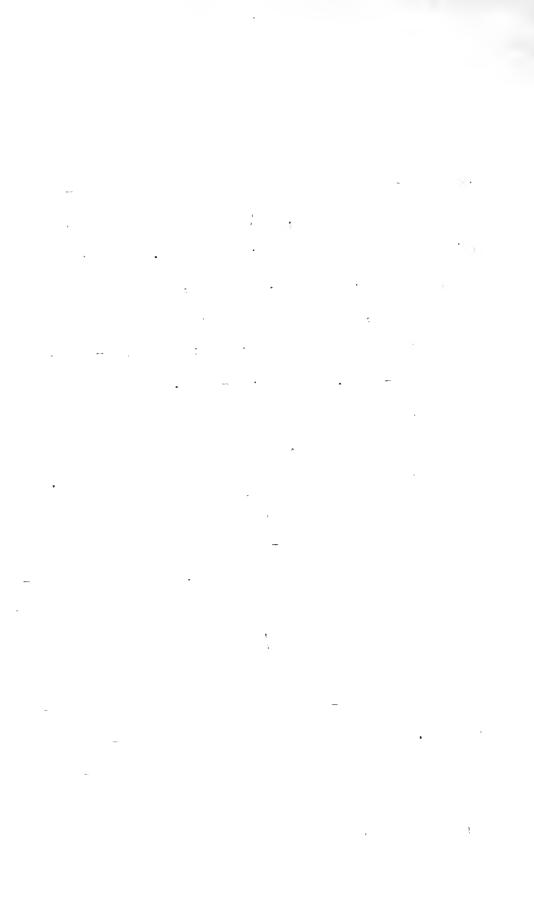
.

The pressure reading taken on the gauge was not the total pressure causing the discharge of the water, but represented the sum of the static and potential heads. According to Bernoulli's Theorem, however, in cases of steady flow, the pressure causing that flow is made up of three factors; viz: velocity-head, potential-head, and static-head. The sum of these three heads at any section of a pipe is a constant quantity, being equal to the sum of the corresponding heads at any other section.

Therefore to obtain the total effective pressure the velocity-head must be computed and added to the gauge reading. This velocity-factor correction is calculated from the formula:

Pv= K^{\dagger} q²

This is worked out on page /0 and a table of the velocity-correction curve points is included. From these points a velocity-factor curve was drawn and correction, was then added to the pressure-discharge curves for each head and the resulting curves drawn. These resulting curves now show



the effective or total pressure, causing the discharge from the sprinkler head.

The Esty and Niagara head curves are found to be smooth, while the Manufacturers head curve has a break occuring at about 40# per square inch pressure. By studing Fig 3, which shows the cross-section of the three heads, it is seen that the Manufacturers head has a much longer shoulder than the other two By the shoulder is meant that part heads. of the head from the top of the orifice to the place where the slight enlargement of the inside diameter occurs. The orifice in all three heads is exactly one half of an inch. Therefore the ratio of the length of the shoulder to the diameter of the orifice is largest in the case of the Manufacturers head and very much smaller in the case of the other two heads. Some experiments have been conducted on similar cases and it was found that if the ratio of the shoulder to the orifice was larger the break would occur at a higher pressure, and if the ratio was decreased, the break would occur at a lower pressure.



This then explains why there is a break in the Manufacturers head curve and apparently none in the case of the other two heads. results of the above named experiment would seem to indicate that a break ought to occur in all cases where there is a shoulder. doubtedly, this is so, but the pressures employed in this test for the low discharges were at one pound intervals until a ten pound pressure was reached, and then discharges at five pound pressure intervals were run. the break in the Esty and Niagara discharge curves occurs at some low pressure below one pound, it was not detected, nor was it attempted to do so, as it wasn't practical or necessary for the purpose of this experimentation.

• . .

SAMPLE CALCULATION

PART 1

Discharge

Total Gallons \$9
Length of run 2 min.
gal. / min. 44.5

Velocity Factor Correction.

$$h = \frac{v^2}{2g}; \quad v = \underline{q}; \quad a = .7854 d^2$$

$$h = g^2$$
 = feet of water $(.7854)^2 \times 64.32 \times d^4$

Changing to pressure in pounds / sq. in the resulting equation is:

Pv=
$$\frac{(.1337)^2 \times 12^4 \times .434 \times q^2}{(.7554)^2 \times 64.32 \times 602} = \frac{q^2}{d^4}$$

Solving: K= .00112625

..
$$PV = .00112625 \times \frac{q^2}{d^4}$$

Where, Pv= pressure correction in 16. 1 sq. in.

q = discharge in gallons / min.

d = diameter of piezometer

Since, d in this case is 0.755 inch.

$$K' = \frac{.00112628}{(.755)^4} = .00346623$$



```
Using the new constant,
```

 $Pv = .00346623 \times q^2$

Vel. Factor Correction applied to curve:

Gallons / min = 44.5

Gauge pressure = 60 lbs / sq.in.

vel. Factor Correction = 6.85# / sq.in.

(from curve)

Effective Pressure = 66.85# / sq.in.

PART 2.

Gauge pressure = 5# / sq. in

Velocity Factor Correction = 1.00# / sq.in.

(from curve)

Effective Pressure = 6# / sq.in.

Total discharge (from curve) = 14.75 gals / min.

Theoretical Q / sector = $\frac{14.75 \cdot = 1.543}{8}$ gal / min.

Weight in pan #1 = 13.5 pounds

Net weight of water = 13.5 - 13 = 0.5 #

Total wt. of water in pan #1

(8 positions) = 13 pounds.

Total water in zone A (6-7-1/2)=

sums of pans, 1, 2, 3, 4

• ٠, • : • • . . . • •

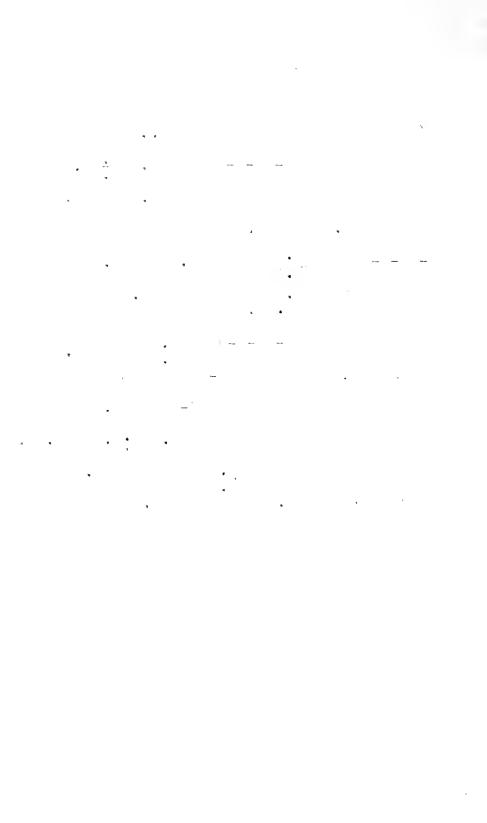
(8 positions) = 50.25 pounds Gallons in Zone $A-(6-7-1/2)=50.25 \div 5.33 = 6.03$ gals.

Gallons / sq.ft / Min. in Zone $A-(6-7-1/2=\frac{6.03}{63.61 \times 5}=.019 \text{ gal.}$ (area of zone 63.61) (run 5 min.)

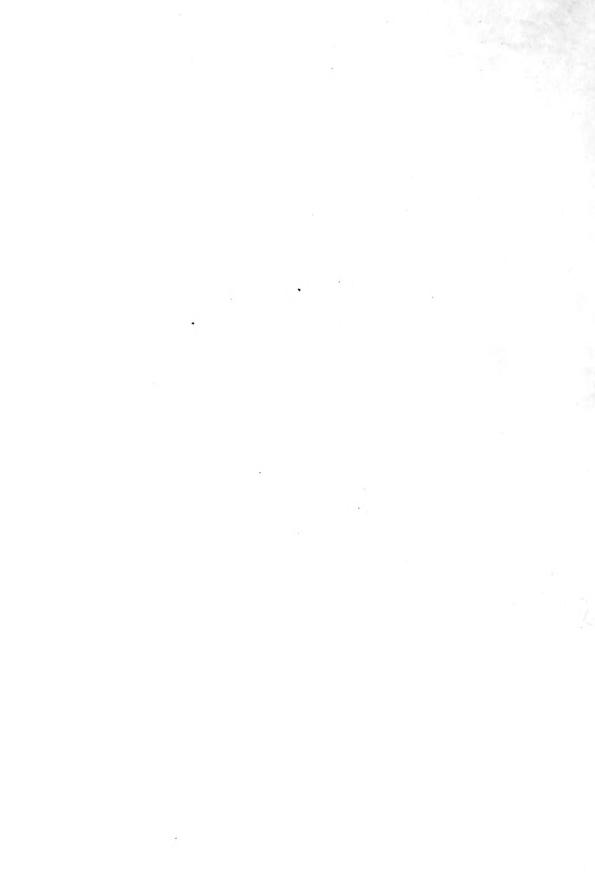
Per Cent in zone $\Lambda = (6-7-1/2) = 6.03 \times 100 = 5.15$ % Total pounds in Sector 1 = Sum of pans 1-12 = 36.45

Total gallons in Sector 1 = 36.45 \$5.33 = 4.37.

Per Cent in Sector $1 = \frac{4.37 \times 100}{1.543 \times 5} = 47.4 \%$ (Theoretical Q = 1.543 gal / min.)



PART 2. DISTRIBUTION.



a) Apparatus.

The apparatus used for this part of the investigation consists of that shown in Fig.

1. A wooden ceiling, 8' x 8', was attached as shown, with the vertical pipe entering 2'

from center and a horizontal pipe of such length as to have the sprinkler head directly under the center of the ceiling. The pressure gauges were arranged as in the illustration.

Directly under the center of the ceiling, on the floor, is an iron base swivel which supports an iron carriage, in the form of a 450 sector, of 7-1/2 foot radius. Therefore, to make a complete revolution about the center point, eight consecutive positions must be taken. A definite sector was taken as No. 1 and the eight sectors were numbered consecutive—ly in a clock-wise direction.

On the sector carriage were placed twelve pans, constructed in such a manner that they covered the entire area of the sector, and would catch all the worker over that area. (See Fig. 2)



A cover of galvanized iron was arranged as in illustration, so that it could cover all the pans when this was desired. (For further details of sector constructions see Rietz & Pfaflins thesis on 'Design of Apparatus for Floor Distribution').

As mentioned above, the sector pans were twelve in number and were numbered for convenience, with No. 1 at left hand of the extremity of sector. No. 2 would be next pan on the left of No. 1. The apex pan would therefore be No. 12.

The twelve pans comprise the sector, while the "zones" are comprised as follows:

Pan No.	Zone	Area Zone in sq.ft.	Distance in ft. from center
1 2 3	A	63.61	6 to 7-1/2
4 \\ 5 \\ 6 \\ 7 \\ 8	В	34.56 28.27	5 to 6 4 to 5



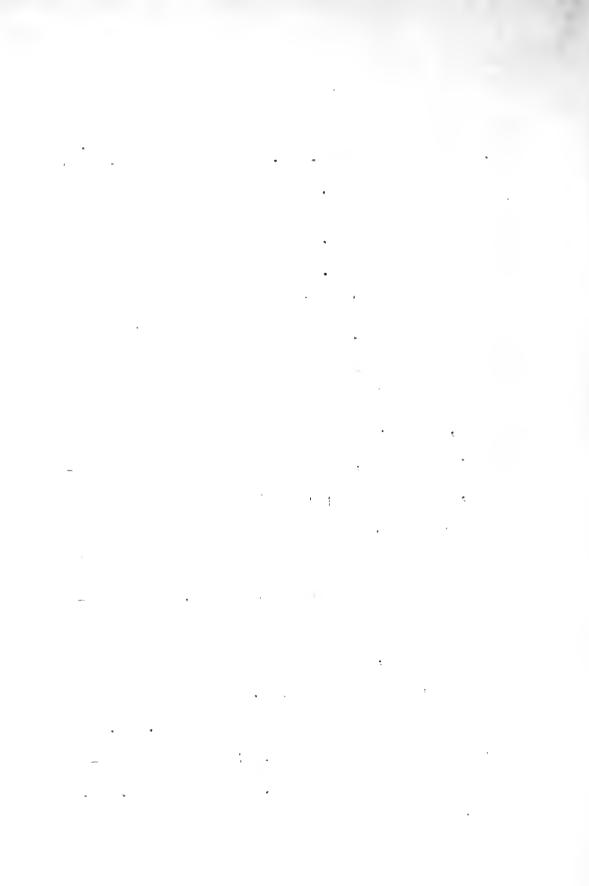
Pan No.	Zone	Area Zone in Sq. ft.	Distance in ft. from center.
9) 10)	D	21.99	3 to 4
11)	E	15.70	2 to 3
12)	\mathbf{F}	12.56	0 to 2

A complete 'zone' consists of the eight sector positions.

b) TEST METHOD

The test was carried on in the following manner, the heads being taken in the following order: The Esty, the Niagara and the Manufacturers, running complete tests on one before taking another.

The sector carriage was set in postion 1 and the cover rolled over the pans. The distance of the deflector from the ceiling was then adjusted to 3", by means of a rachet connection placed under center and the head, of the ceiling. The pressure was then turned on and adjusted to 5# / sq. in. true pressure and when constant, the cover was removed and the pans exposed. For 5# / sq. in. pressure the run was of 7 minutes duration



while for other pressures it was of 5 minutes duration. At the end of the period, the cover was pulled back over the pans and the water turned off. A run constituted the time from which the sector was just uncovered to the time when it was just being covered, the covering and uncovering being done in the same direction and at the same velocity. When the dripping from the ceiling had ceased the cover was removed and each pan weighed separately and the data recorded.

The tase weight of the pans were as follows:

No.	Wt. in Lbs.	No.	Wt. in Lbs.
1	13.00	7	12.50
2	12.75	8	12.80
3	12.75	9	10.60
4	12.75	10	11.25
5	14.4	11	14.00
6	14.75	12	13.50

Runs were next made at 25# / sq. in. and then at 50# / sq. in. pressure.

ţ .

. . .

• •

The head was then adjusted to 6" from the ceiling and pressures of 5#, 25# and 50# / sq. in. taken as above.

The process was then repeated with the deflector 10^n from ceiling.

This completed the investigation for the Esty head.

The same test runs were then made with the Niagara and Manufacturers heads.

From this data, calculations were made as in accompanying sample. Calculations and the "zone distribution" and "sector distribution" curves were plotted.

In plotting the former, the zone in distance from center in feet was used as the abscissa and the gallons per sq. ft. per minute as ordinate, for each pressure and each position from the ceiling.

In plotting sector distribution curves, the following method was employed. Instead of using rectangular coordinates, concentric circles were employed to represent percentages. The circles were divided into the eight equal sectors. On these sector lines, the



percentage of the actual discharge to the theoretical was laid off. By connecting these points, the sector distribution of the head at that particular pressure and distance from the ceiling was shown.

c) Discussion and Results.

Upon examination of the zone distribution curves the following facts are evident:

For the 5# per square inch observed pressures and different positions of deflector from ceiling, most of the water is distributed over zones F and E. The remaining zones receive a very much smaller though relative—

ly uniform distribution.

For the 25# per square inch observed pressures and different positions of deflector from ceiling, the distribution is greatest and somewhat uniform in zones F, E and D. In the remaining zones the distribution decreases as the distances from the center increase.



For the 50# per square inch observed pressure and different positions of deflector from ceiling, the distribution is more uniform throughout all zones than in the previous two pressures.

The amount of water thrown outside the pans is lowest for the 3 inch position of the deflector from the ceiling and increases as the distance from the ceiling is increased.

Upon examination of the sector distribution curves the following facts are evident:

For the 5# per square inch observed pressure and different positions of the deflector from the ceiling, the sector distribution was relatively uniform, averaging about 80%.

For the 25# per square inch observed pressure and various positions of deflector from ceiling, the sector distribution is less uniform, averaging about 90%.

For the 50# per square inch observed pressure and various positions of the de-flector from the ceiling the sector distribution is quite varied.



PART

-3-

CONCLUSIONS.

•		

A zone distribution curve that approaches a straight line and has the greatest percentage of water within the zones, is the ideal curve. When a zone distribution curve approaches a straight line it demonstrates that the distribution per unit area is equal throughout the entire floor space.

A sector distribution curve is best when the curve is a regular octagon with its points on the 100% circle. A curve of this nature shows that an equal amount of water was discharged into each sector and the percentage less than 100 is the quantity which fell outside of the pans.

The following heads are considered to have the best zone and sector distribution curves, under the conditions mentioned:

3 inch position and 5# pressure

Zone Distribution - Manufacturers.

Sector " - Esty.

	,			
~				
	• · · · · · · · · · · · · · · · · · · ·			
		•		
(4)	\$ 			
, **				
-1			,	
5.				

```
3 inch position and 25# pressure.
Zone distribution
                               Niagara
Sector
                               Manufacturers.
          3 inch position and 50# pressure.
Zone distribution
                                Esty
Sector
                                Niagara.
          6" position and 5# pressure.
Zone distribution
                               Manufacturers
Sector
          6" position and 25# pressure
Zone distribution
                                Niagara
Sector
                                Manufacturers
          6" position and 50# pressure
Zone distribution
                                Esty
Sector
         10" position and 5# pressure
Zone distribution
                                Manufacturers
Sector
                                Esty
         10" position and 25# pressure
Zone distribution
                                Niagara
Sector
                                Manufacturers.
```



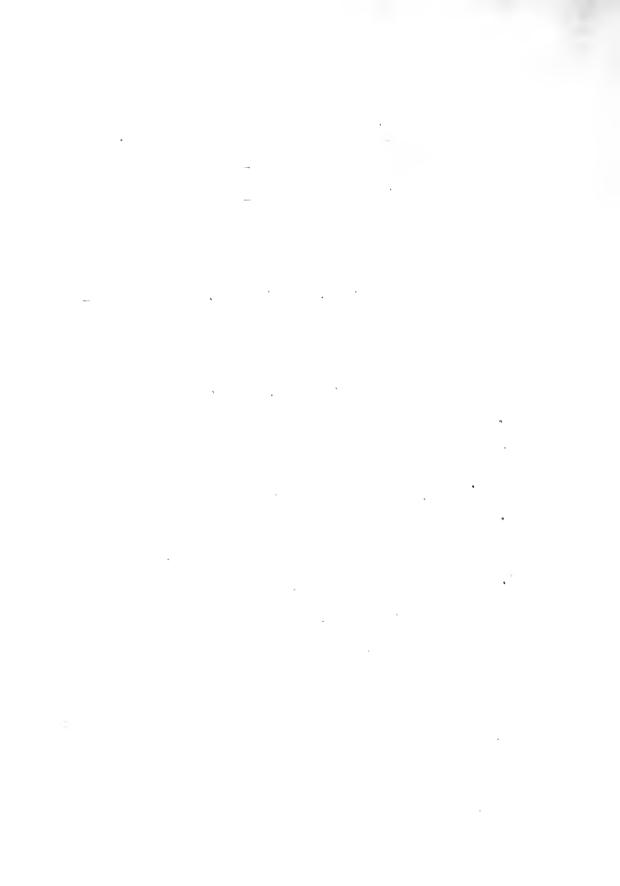
20ne distribution - Niagara
Sector - Niagara

The results obtained may be checked only when all the conditions of the original test are duplicated in the check run. The following are some of the conditions which may be easily overlooked and yet which have a definite bearing on the results obtained:

- 1.) Position of the pipe holding the test head and through which water was supplied to the head.
- 2.) Position of the arms of the test head with respect to the pipe mentioned in (1).
- 3.) Location of sectors.
- 4) Service Pressure.

The above conditions will be more clearly understood when each of the above conditions is considered as applying to each head separate-ly:

1) The pipe holding the test head was pointing east and West coming through the ceiling



in the western half and terminating under the center of the ceiling. This condition was constant for all three heads tested.

2) In testing the Esty head, the head was screwed in tight, with the arms perpendicular to a vertical plane through the supply pipe.

The Niagara head was tested with its arms in the same vertical plane of the supply pipe.

The Manufacturers head was tested with its arms making a 60° angle, in a counter clock-wise direction, with the vertical plane of the supply pipe.

3) This vertical plane of the supply pipe was the division line between sectors 1 and 8. Sector 1 was therefore under the eastern half of the stand and south of the vertical plane of the supply pipe. The sectors were then numbered consecutively in a clock-wise direction.



4.) Such tank pressures were used as would give the most steady flow for the required When the heads were run at discharge pressure. 50# per square inch discharge pressure, the service pressure was kept at about 100# / sq.in. For the 25# discharge pressure, the test was made with the service pressure at about 80#. the 5# discharge pressure, the run was made at about 60# service pressure. These were the same for all the heads. The above named service pressures gave a steady discharge without much variation in the discharge pressure, thereby making it easy to hold a constant discharge pressure during the length of run.

If the above named conditions are not duplicated in checking the results, the following differences in results will be obtained.

A change in condition (1) or (2) will make a difference in the amount of water in each sector, although the total amount in all eight sectors would remain the same. These results would give different sector and zone distribution curves for the heads. A change in condition

⁽³⁾ would not affect the zone distribution curve but the relative position of the sector distribution curve would be changed. A change in condition (4)

. * .

would make it difficult to keep the discharge pressure uniform and, therefore, would change the amount of total discharges. The general appearances of the curves would be very little affected.

				,	
					77.13
		;	1:		ť a
	•				
			•	· · · :	
			,	•	
					·.
					1
					. ,



Fig.1. General View of Apparatus.





Fig.2.
Pans Uncovered.

1).	

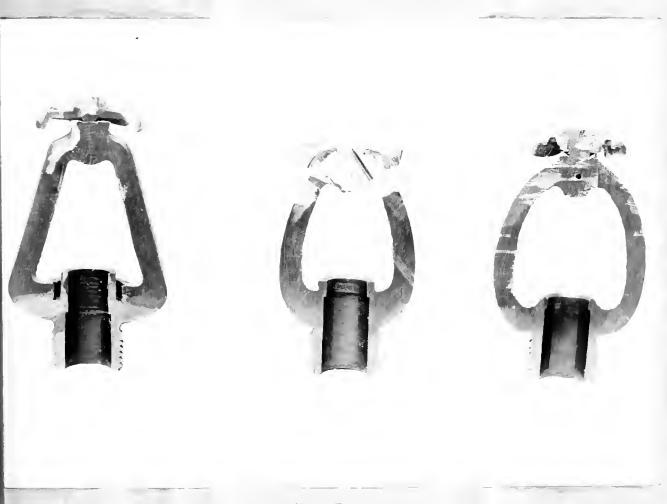


Fig.3.

Manufacturers Esty Niagara

Cross-Sectional View of Heads.



....

. . .

Gauge Calibration Data.

Gauge #60 Model	K
Foxboro	
0 - 50	

Gauge #61 Model K
Foxboro
0 - 200

True Press	• Qbs. Press.	True Press.	Ohs Press
5	5.50	25	27.00
10	10.75	30	30.00
15	15.75	35	35.00
20	20.5	40	40.50
25	25.75	45	45.00
30	30.75	50	51.00
3 5	35.50	55	55.00
40	40.75	60	60.00
45	45.75		
50	50 x		

					4	
	•					
	dam ng			•		
		•	•	•		
•	1					
•			•			
		0				
•						
					•	
100			•			
	,					
			•			
*						
•			•			
			•		'	
,						
*			•			
•			•			
			•			
					•	
•						
*						

VELOCITY FACTOR CORRECTION DATA.

Points Calculated for velocity factor correction curve from equation:

 $Pv = .00346623 \times Q^2$

Gals / Min.	Lbs. / sq. in.
<u>Q</u>	Pv
5	.0866
10	•3466
15	•7799
20	1.3564
25	2.1664
30	3.1196
35	4.2460
40	5 • 5459
45	7.0190
50	8.6655
55	10.4850
60	12.4784

•

•

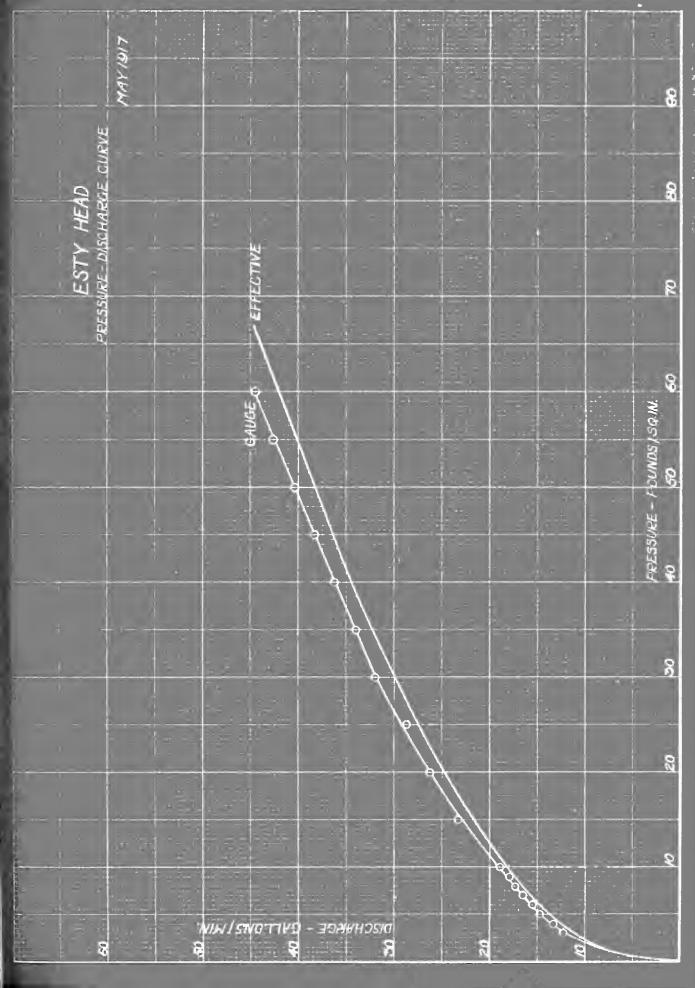
•

•

•

TRANSPORTOR OF LANDONS DE	713	
\	DIAMETER OF PIEZOMETER	e = 0.755 /N. MAY 1.977
We) (en		
077IVO - 30		
September 1		
8		
9		
	2 S + FOUNDS/SQ.M. 5 S	0





	1
in the second se	

RVE MAY 1917		8
NIAGARA HEAD PRESSURE DISCHARGE CURVE		90
NIAGARA PRESSURE DISCH	→ EFFECTIVE	ez.
	ONNGE	POUNDS / 56 IN 50 60
		PRESSURE -
		8
		20
		Q
\$ E	PISCHARCE CALLONS/MIN	Jan



MANUFACTUREES HEAD PPESSUPE-DISCHARGE CURVE	718/ YAM	— EFFECTIVE			06 08
		OAUGE O			PRESSURE - POUNDS / SG. IM.
				2	95
93		פענד מעזפ / געני	оюсну <i>в</i> ее.		10 20



BSTY HEAD

GAUGE PRESSURE, 5 lbs. sq. in; DEFLECTOR 3" FROM CEILING; EFFECTIVE PRESSURE, 6 lbs. sq. in. 5 min. runs.

66	in Zone	8.18	5.78	7.70	10.40	19,23	20.75	
8	Sq.Ft.Min.	.019	.0247	.042	8690.	.181	. 244	
- A	In Zone	6.03	4.26	4.68	7.67	14.20	15.30	
Weight	in Zone	A- 50.25	B- 35.55	0- 47.35	D- 63.95	E-118.25	F-127.75	
Total	Weight	13.00 14.00 12.75	17.55	26.00 c	32.95 31.00	118.25 E	127.75 E	
	VIII	2.00 1.75 1.75 2.25	2.10	3.75	4.15	9.50	14.00	
	VII	2.00 1.25 0.75	2.35	3.50 3.20	3.90	14.00	18.50	
	VI	1.00 2.75 2.00	3.25	4.50 3.20	6.90	22.00	14.75	
이 제 81	Λ	1.75 2.50 2.25 1.25	2.85	3.00	3.40	15.00	19.50	
터 이 테	ΙΛ	2.00 1.75 1.75 2.00	2.10	2.50	2.90 4.25	21.50	15.00	
ळो	III	2.50 1.25 0.25 0.26	2.60	3.50	4.40	14.00	18.50	
	II	1.25 1.50 1.50 0.25	2.10	3.25	5.40	13.25	20.00	
	н	0.50 1.25 1.75	1.60	2.00	1.90	00.6	7.50	
	PANS	1004	ပ သ	r 00	901	11	12	Total

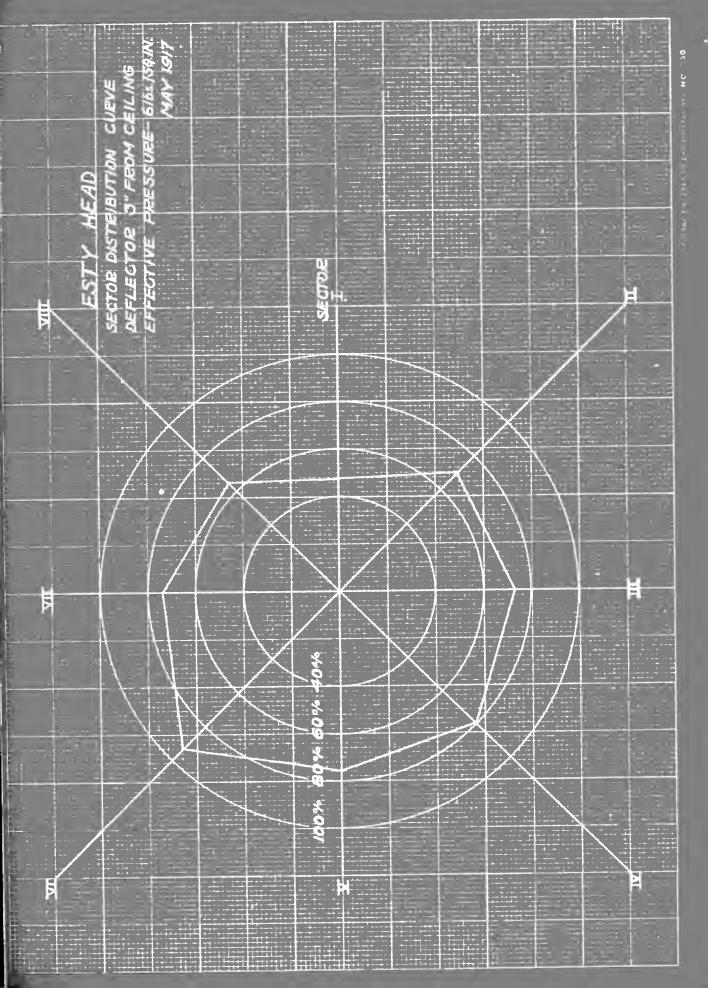
14.75 Gals. QSector 1.843 1.843 1.843 1.843 1.843 1.843 1.843 1.843 36.45 54.20 55.70 61.20 58.45 71.45 57.70 49.95 00.9 6.83 7.35 7.02 8.57 6.68 6.50 4.37 Total Gallons Pounds

72.04

47.4 70.5 72.4 79.8 76.1 93.0 74.0 65.1 % in Sector

9		2113		ZONE DIS DEFLECT	BUTION CURVE S'FROM CEILING
52				EFFECTIV	VE PRESSURE - 6 Iba Nº 1817
.NIM					
já ,π=1ρε\ 2					
פעררסא פ					
50.	72.04%				
٥	F Z E S	CE FROM C	C S B	7	712 27.96%

	5





ESTX HEAD

GAUGE PRESSURE, 25 lbs. sq. in; DEFLECTOR 3" FROM CEILING; EFFECTIVE PRESSURE, 28.5 lbs. sq. in. 5 min. runs.

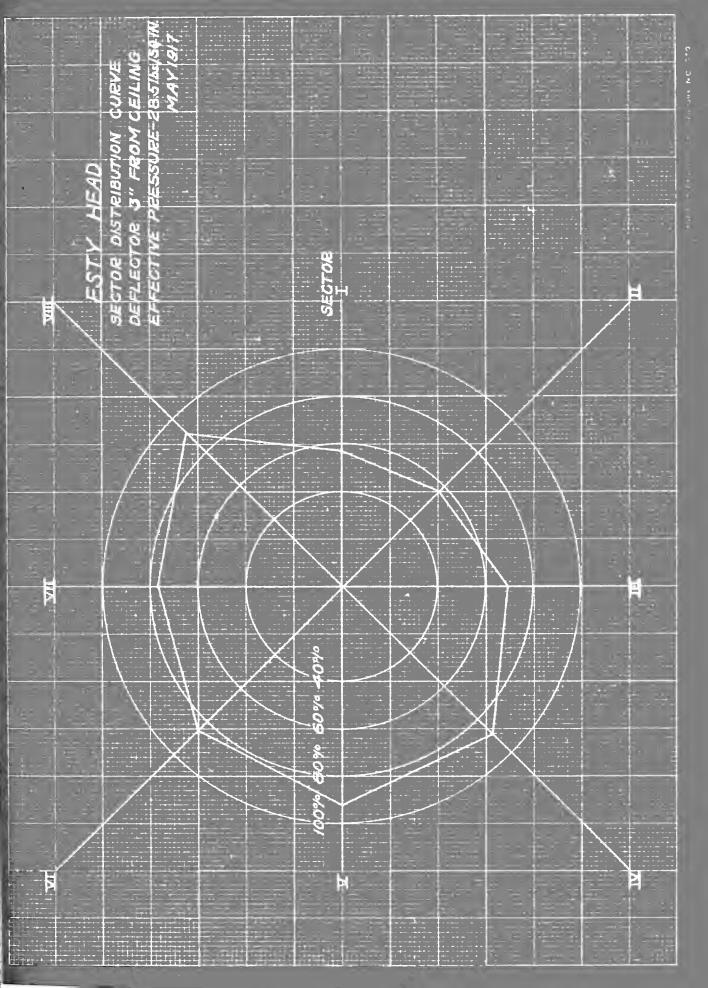
10° 2	Zone	6.	8.75	14.21	21.5	14.2	9.48	77.4
Gals.		.0428	.0742	.147	. 284	.262	22.	
Gals.		13.6	12.8	80.8	31.2	20.5	13.86	
Weight	Zone	A-113.50	B-106.55	C-173.60	D-259.70	E-170.50	F-115.50	
Total	210101	25.25 30.00 33.25 25.00	58.05 48.50	93.75 79.85	134.20 125.50	170.50	115.50	139.70
	VIII	5.00 4.25 5.25 4.00	11.60	15.50 12.20	20.40 25.25	21.50	00.9	116.95
	VII	3.50 2.75 1.75	5.60	7.50	21.90	36.50	18.00	129.45 11
의 의 의 의 의 의 의 의	IA	2.00 3.25 4.75	6.10	8.50	13.40 22.75	28.00	18.00	20 129
	Λ	4.50 7.25 8.25 3.75	9.60 11.25	15.50	18.90 16.50	9.50	17.50	95 140.
	IΙ	4.50 5.75 5.75 5.25	9.60	15.00	24.90 17.25	7.00	9.50	134.95
	III	4.00 1.75 0.50 0.25	5.10	16.75 4.95	19.90	25.50	20.00	104.20
	II	0.75 1.25 1.75 1.50	2.35 3.25	4.50	7.90 14.25	29.00	15.50	87.20
	H	1.00 3.75 5.25 4.25	8.10	10.50	6.90	13.50	11.00	86.70
	PAMS	ч ак4	လ သ	8	901	11	12	rotal Pounds

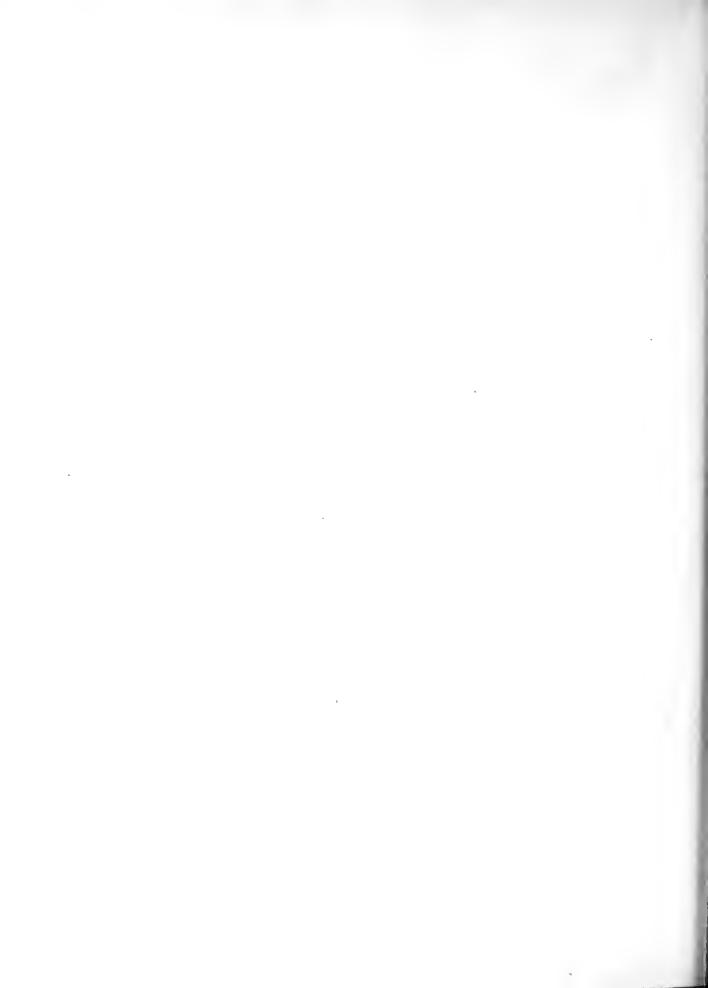
29.25 Gals. QSector3.656 3.656 3.656 3.656 3.656 3.656 3.656 3.656 16.8 15.54 14.05 16.75 16.2 10.46 12.5 Total Gallons10.4

% in Sector 56.9 57.2 68.4 88.7 92. 85.1 76.8

.

EAD	BUTION CURVE 3" FEOM CEILING PRESSURE-28,516,159 IN MAY 1917			26%
ESTY H	ZONE DISTRIBUTION CURVE DEFLECTOR 3" FROM CEILIN EFFECTIVE PRESSURE-28.5			72.2.7
				TER-FEET
				ANCE FROM CENT
			* * *	ZONE-DIST
Control of the latest to		אדד מאפ לפט וב פי	25 277.44%	e li





BSTY HEAD

GAUGE PRESSURE, 50 1bs. sq. in; DEFLECTOR 3" FROM CEILING; EFFECTIVE PRESSURE, 55.5 1bs. sq. in. 5 min. runs.

₩.H	27	11.23	15.54	17.96	13,75	11.85	7.91	
Gala. So.Ft.Min.		.0715	.182	. 257	. 253	.306	. 255	
Gals.	,	22.75	31.48	36.37	27.86	24.	16.02	
Weight	Zone	A-189.25	B-262.3	G-303.1	D-232.2	E-200.	F-133.5	
Total Waisht	210	42.0 44.0 56.0 47.25	109.8	165.5 137.6	134.2 98.0	200.	133.5	
	İIIA	10.25 11.75 11.25 11.25	19.6 30.75	33.0 30.2	25.9 11.25	19.0	12.0	
	VII	7.75 2.75 2.25 1.75	17.1 6.25	23.5	15.4 11.25	51.0	28.0	
	IA	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7.6	13.50	15.9	23.5	18.0	
S H O E S S H S S	Λ	5.5 9.75 13.75 8.75	19.1 28.75	83.5 83.5	14.4 9.25	10.5	23.0	
	ΙΛ	8.0 10.75 10.25 8.75	20.6 35.75	32.0 13.2	11.9	9.5	13.0	
	III	7.0 1.75 0.75 0.25	19.1	26.0	23.4	34.0	18.0	
	11	1.75	4.25	0.8 12.8	16.4	31.50	14.5	
	н	1.0 8.25 8.55	3.60	7.50	10.9	21.0	7.0	
	PANS	1884	က တ	8 4	9	11	12	

Total Pounds 124.20 123.95 145.95 179.45 189.45 157.45 173.70 226.20

78.24

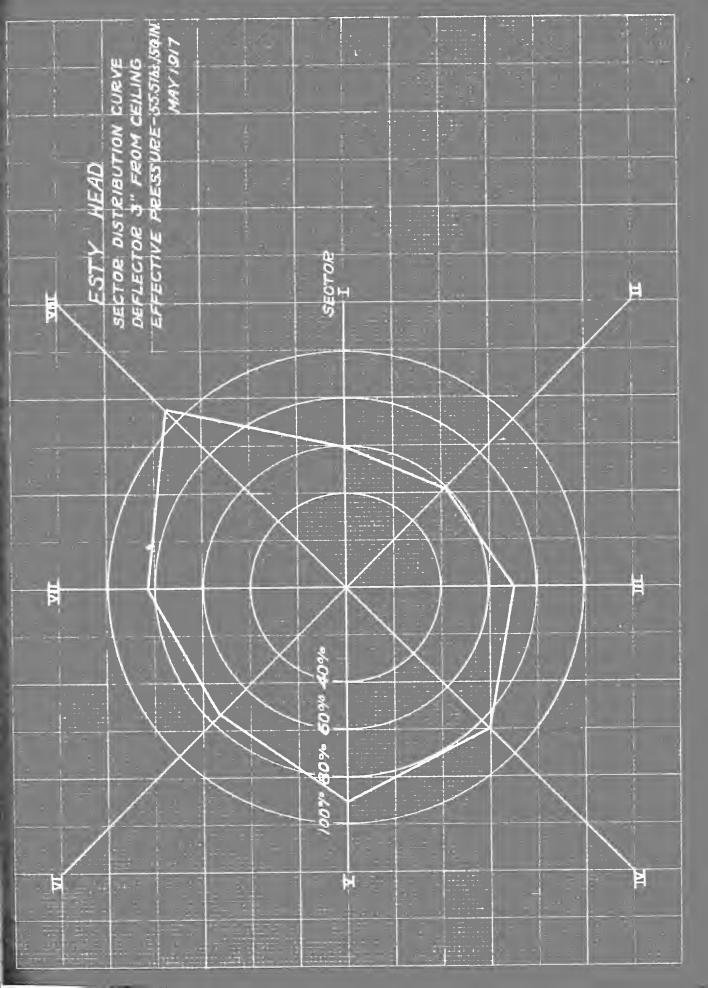
20.85 27.15 Total Gallons 14.90 14.87 17.50 21.55 22.75 18.9 40.5 Gals. QSector5.0625 5.0625 5.0625 5.0625 5.0625 5.0625 5.0625 5.0625

58.8 58.7 69.2 85.2 90.0 74.7 82.4 107.3 % in Sector

•

	OURVE M CEILING RE- 355 Ibs. /SRIK MAY 1017						
ESTY HEAD	ZONE DISTRIBUTION CURVE DEFLECTOR 3" FROM CEILING EFFECTIVE PRESSURE- 35.5 16: SRIN.					21.76%	7/12
							<i>₹</i>
							e-FEET S B
							OM CENTES
							ZONE - DISTANCE FROM CENTER - FEET
							ZONE- DIS
						78.24 %	ų.
30	2	NIWI	⊥	ארד <i>סא</i> פ	ET	55	0

*	





HEAD 지 테 의 얼

GAUGE PRESSURE, 5 lbs. sq. in; DEFLECTOR 6" FROM CEILING; EFFECTIVE PRESSURE, 6 lbs. sq. in. 5 min. runs.

12 %	Zone	8.75	6.30	8.37	10.44	14.76	18.30	66.92	
Gals.	F .	.023	.0269	.0436	.00	.139	.215		
Gals. In Zone		6.45	4.65	6.17	7.7	10.88	13.5		
Weight	Zone	A- 53.75	B- 38.80	C- 51.45	D- 64.20	E- 90.75	F-112.50		
Total Weight		13.75 15.00 14.25 10.75	19.55	26.50 24.95	33.95	90.75	112,50		
	VIII	2.00 1.25 1.75	2.10	3.75	4.40	9.50	11.50	47.20	5.66
	VII	2.00 1.25 0.75 0.75	2.60	3.00	3.40	00.6	18.00	50.95	6.11
	VI	1.00 3.25 3.00 1.75	3.25	5.00	6.90	16.50	11.00	63.70	7.64
이 때 의	Λ	200 200 200 200 200 200 200 200 200 200	2.60 2.25	3.00	3.40	10.00	20.50	53.95	6.48
의 의	IΛ	200 200 200 200 200 200 200 200 200 200	2.60	2.95	2.90	12,25	16.50	56.45	6.77
ଅ	III	3.00 1.50 0.75 0.25	2.60 1.25	3.50	5.65	11.00	15.50	52.20	6.27
	II	2.00 1.75 0.50	2.35	3.50	5.40	14.50	13.50	51.95	6.23
	Н	0.50	1.60	2.00	1.92	8.00	00 • 9	34.95	4.2
	PANS		യവ	8	9	11	12	Total Pounds	Total Gallons

14.75 Gals.

QSector1.843 1.843 1.843 1.843 1.843 1.843 1.843 1.843

73.4 70.3 82.8 66.3 61.4

% in Sector 45.6 67.5 68.

- . .

.

AD	ION CURVE FROM CEILING SSURE - 616, 1581N. MAY 1917						8%
ESTY HE	JE DISTRIBUT FLEGTOR 6" FECTIVE PRE						A 33.08%
							8
							CENTER-FEET
							5 4
							ZONE - DISTANCE FRO
						67.92%	u
30		5 B.I	'NIM	, । प्रमः १८ ।	0477 <i>0</i> 9	95	0

*		4.
	6	
·		
•		
		1

ESTY HEAD

GAUGE PRESSURE, 25 lbs. sq. in; DEFLECTOR 6" FROM CELLING; EFFECTIVE PRESSURE, 28.5 lbs. sq. in. 5 min. runs.

<i>₽</i> € *	Zone	ى ئ	8.6	17.37	18.55	11.66	9.56		76.44	
Gals.	• HTH• • 0.2 • 10 C	.0436	.083	1795	.247	.217	. 223	1	4	
Gala.		13.88	14.34	25.4	27.15	17.05	13.98			
Weight	Zone	A-115.50	B-119.55	C-211.85	D-225.95	E-142.	F-116.50			
Total	A TRATEM	28.00 28.25 32.00 27.25	58.30 61.25	98.50 103.35	107.20	142.00	116.50		150.45	
	VIII	7.50 6.75 5.75 3.75	13.60 10.25	17.00	17.40 20.75	24.00	8.00			
	VII	3.00 1.75 1.25 1.25	5.60	8.50	22.90	22.00	17.50		95 99.45	
	ΙΛ	2.00 2.75 5.25 4.75	6.10	8.00	7.90	20.50	10.50		20 111.95	
0 되 입	٨	3.50 6.00 8.75 6.00	9.10	17.00	14.90 14.50	9.50	22,50		145.	
티 이 떼	IV	6.50 6.75 5.25 4.75	13.10	19.50 23.70	19.90	10.50	10.50		142.95	
ળા	III	4.00 1.25 0.25 0.25	6.10	21.50 4.70	12.90	25.50	16.50		98.95	
	II	0.50 1.25 2.75 1.75	2.10	3.50 7.20	7.40	16.50	18.00		88.95	
	н	1.00 1.75 2.75 4.75	2.60	3.50	3.90	13.50	13,00		83,45	
	PANS	100 to 4	တ သ	8	9	11	12		Total Founds	

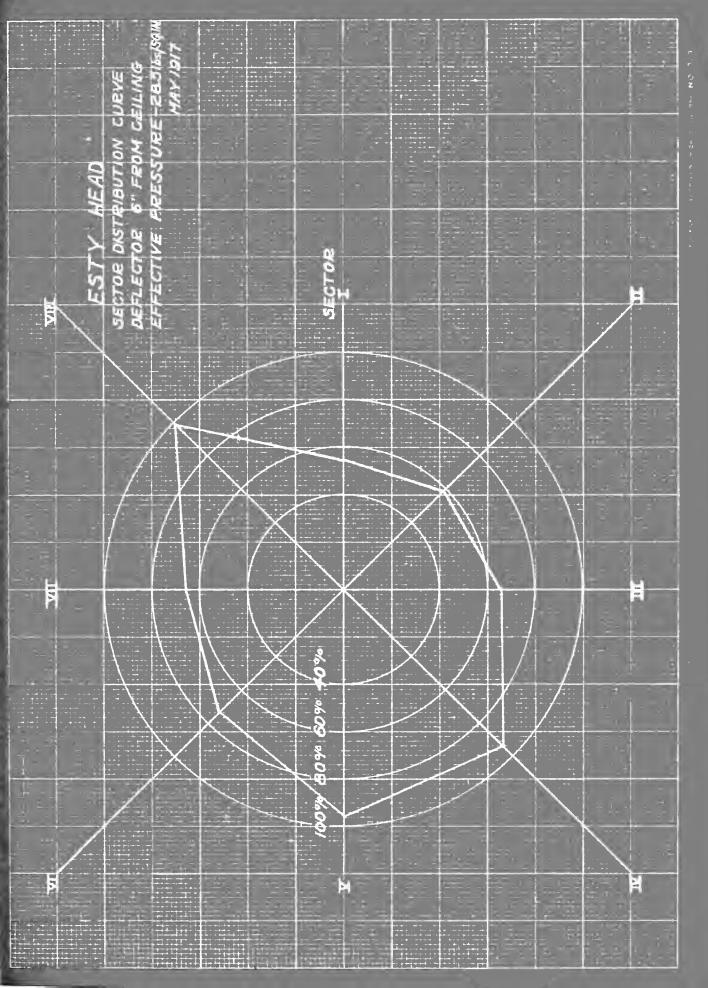
29.25 Gals. QSector3.656 3.656 3.656 3.656 3.656 3.656 3.656 3.656 17.15 17.43 13.45 11.93 18.05 Total Gallons10.01 10.67 11.9

65.16 98.8 73.6 95.5 65.15 93.9 % in Sector 54.75 58.4

. •

ESTY HEAD	ZONE DISTRIBUTION CURVE DEFLECTOR 6" FROM CEILING EFFECTIVE PRESSURE-ZBS/As/30/A. MAY 1917		23.56 % Tree
			DISTANCE FROM GENTER-FEET
35°	3	S/SNOTTV9	36 76.449% ZONE - DI

•		





RSTY HRAD

GAUGE PRESSURE, 50 lbs. sq. in; DEFLECTOR 6" FROM CEILING; EFFECTIVE PRESSURE, 55.5 lbs. sq. in. 5 min. runs.

P6 2	Zone	12.68	16.58	17.9	12.85	9.83	8.63	
Gals.	77 77 77 77 77 77 77 77 77 77 77 77 77	.0807	.1943	. 2565	.2367	.2540	.2785	
Gals.	2103	25.69	33.58	36.25	26.03	19.92	17.49	
Weight	Zone	A-214.05	B-279.8	0-302.1	D-216.95	E-166.	F-145.75	
Total Weicht	910	45.80 52.00 63.5 52.75	115.8 164.0	164.5 137.6	123.45 93.5	166.	145.75	
	VIII	11.0 13.75 12.75 10.75	19.60 32.00	29.5	21.9	20.00	11.50	
	VII	7.0 2.75 1.75	17.10	24.5	16.90	36.50	28.00	
	IV	1.5 4.25 7.25 5.25	8.10	13.0 32.95	13.90	16.50	17.00	
0 되 3	A	4.5 9.75 14.25 9.25	18.35	20.5	14.4 8.75	11.50	20.00	
	ΙΛ	13.3 15.25 13.75	25.60 39.25	34.0	12.4	11.00	18.50	
Ø	III	200000000000000000000000000000000000000	19.1	26.5	18.4	29.00	22.25	
	II	0.75 2.00 3.00 1.75	2.85	6.5	14.65 24.25	24.50	19.50	
	н	0.75 2.25 10.25 11.75	5.1 34.25	10.00	10.9	17.00	00.6	
	PANS	10x 20 4	စ ည	8.4	9	11	12	F 0+0F

Total Pounds 129.70 121.70 142.45 218.25 178.95 151.70 159.20 222.70

78.47

26.7 21.45 18.2 19.1 Gallons 15.56 14.6 17.1 26.2 Total

QSector5.0625 5.0625 5.0625 5.0625 5.0625 5.0625 5.0625 5.0625 5.0625 40.5 Gals.

67.6 103.6 84.8 71.9 75.5 105.5 57.7 61.5 % in Sector

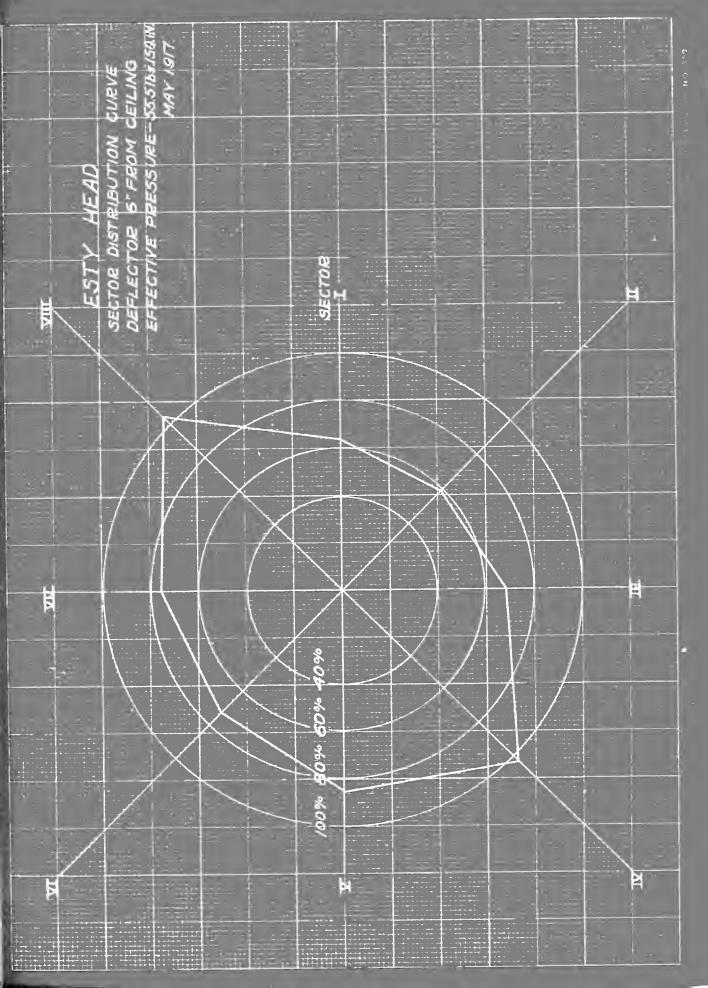
•

. . .

.

.

W CURVE	M CEILING ORE - 55,516=1591N MAY 1977									
ESTY HEAD ZONE DISTRIBUTIO	DEFLECTIVE PRESSURE - 55 516.1591N							(21.53%	A 77%
										v
										FEET S
										OM CENTER-FEET
				, j						CE FROM
				1 2						- DISTAN
						F		.	%	ZONE Z
									78.47	N.
8		25	02		ρ 13. φ ε	l swa	9 9		ફ	0





ΑI 전| 전| 四 **|** 티 의 테

GAUGE PRESSURE, 5 lbs. sq. in; DEFLECTOR 10" FROM CEILING; EFFECTIVE PRESSURE 6 lbs. sq. in. 7 min. runs.

50	in Zone	11.9	10.34	13.9	14.6	11.1	14.78	76.62	
G	Sq.Ft.Min.	.0276	.0442	.0727	860.	.104	.1215		
~	In Zone	12.3	10.66	14.37	15.08	11.46	15.24		
Weight	in Zone	A-102.50	B- 88.80	0-119.85	D-125.70	E- 95.50	F-127.		
Total	Welgnt	31.25 24.00 21.00 26.25	46.30 42.50	63. 7 5 56.10	69.70	95.50	127.00		
	VIII	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	7.60	14.50 13.20	18.65	10.25	8.25	95.80	
	VII	4 % % % % % % % % % % % % % % % % % % %	4.60	4.50	4.90	14.50	18.25	78.45	
	ΙΛ	4.55 4.75 4.25 4.25	6.60	8.00	7.65	10.50	13.50	86.70	
0 R SI	Λ	4 % % % % % % % % % % % % % % % % % % %	4.60	5.25	5.65 8.50	7.75	31.00	74.20	
티 의 ബ	IV	2.50 1.50 1.25 1.75	7.10	13.50	12.65	13.00	19.25	97.20	
थ।	III	4.25 2.25 2.75 4.25	4.10	4.95	3.40	10.00	10.00	64.45	
	II	4.00 3.75 3.25 3.75	6.10	7.50	8.90	18.00	14.25	89.20	
	н	4.75 3.25 2.50 3.75	5.60	6.50	7.90	11.50	12.50	73.95	
	PANS	Lのひみ	တ္ သ	4	9	11	12	Total Pounds	Total

9.41 11.48 7.73 11.66 8.9 10.4 8.88 10.7 rotal Gallons

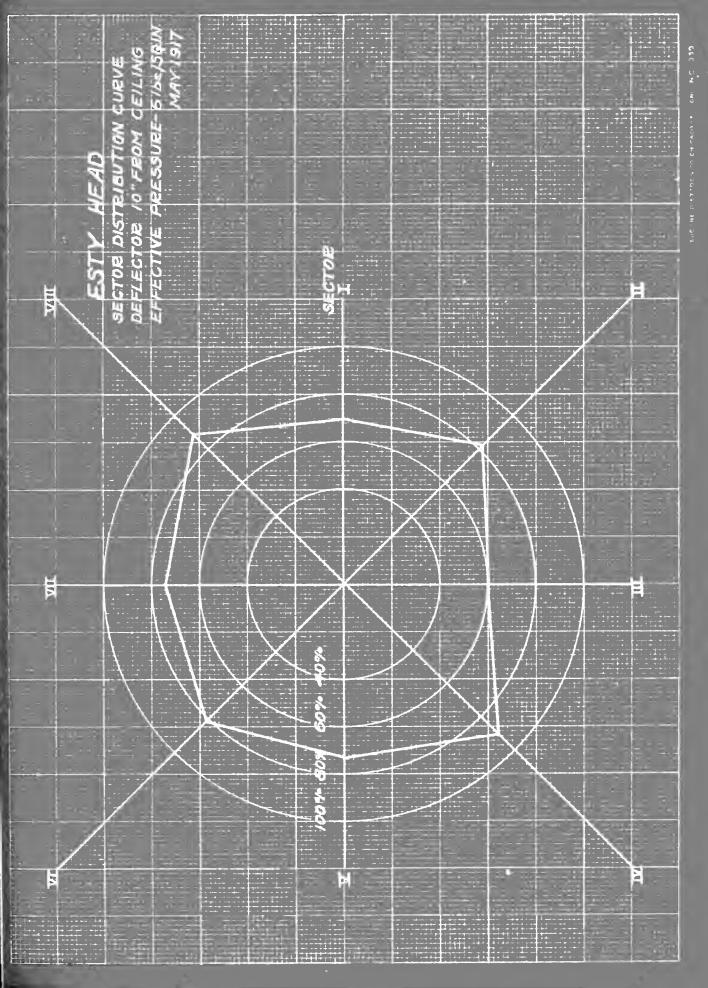
14.75 Gals. 1.843 1.843 1.843 1.843 1.845 1.843 1.843 1.843 QSector.

83. 68.8 % in Sector

88.5 72.9 80.7 71.8 90.4 59.6

	1NG SQ1N. Y Q17						c
	N CURVE FOM CELL SURE-61						
TY HEAD	ISTEIBUTIO TOR IO" F IVE PRES						23.38% 7%
ESTY	ZONE DISTRIBUTION CURVE DEFLECTOR 10" FROM CEILING - EFFECTIVE PRESSURE-616-1591N. MAY 1917					Ĭ.	₹
							IQ
							CENTER-FEET
							FROM CEN
							DISTANCE !
							ZONE- DI
						76.62 %	i .
	2	2	ל בבן אומי פ	שרר סאפ <i>רפ</i> 2	9	8	o

*/	
	,
(542)	
	2
	·



	*	•

Al Ψ١ ध्या 田 إ**ا**< 12 ۱ ال

GAUGE PRESSURE, 25 1bs. sq. in; DEFLECTOR 10" FROM CEILING; EFFECTIVE PRESSURE, 28.5 1bs. sq. in. 5 min. runs.

50 7	Хоре	11.97	12.94	15.50	16.60	13.47	10.63	
Gals.	• TTTW • 0 - 3 • 5 C	.055	•109	.16	.221	.251	.2475	
Gals.		17.5	18.9	22.65	24.5	19.7	15.54	
Weight	Zone	A-145.75	B-157.55	C-188.85	D-203.65	E-164.25	F-129.50	
Total Weicht		38.00 38.00 37.75 32.00	80.80	99.00	113.95	164.25	129,50	
	VIII	3.75 3.25 3.75	10.60	11.50	16.90	14.00	13.50	
	VII	5.25 3.25 2.25 2.75	7.60	9.00	12.40	27.50	16.50	
	IA	4.00 5.50 4.25 2.25	9.60	15.00	15.40	20.50	12.25	
이 ബ ଆ	Λ	3.00 2.75 3.75 2.00	5.35 4.25	8.50	13.40	19.00	36.50	
티 의 폐	IV	7.25 6.25 5.25 4.00	14.10	11.75	14.90 9.25	21.00	20.50	
1	III	4.50 4.25 3.50 4.25	7.35 8.75	7.50	6.90	17.50	11.25	
	II	4.75 7.25 8.75 4.75	14.60 16.00	19.25	16.90	26.00	11.00	
	Н	5.50 6.25 8.25	11.60	16.50	17.15	18.75	8.00	
	PANS	ч ака	က တ	8	10	11	12	

Total Pounds138.95 163.95 102.65 135.20 110.95 117.45 110.95 110.95

Gallons16.68 19.68 12.3 Total

29.25 Gals. 3,656 3.656 3.656 3.656 3.656 3,656 QSector3.656 3.656

13.3

13.3

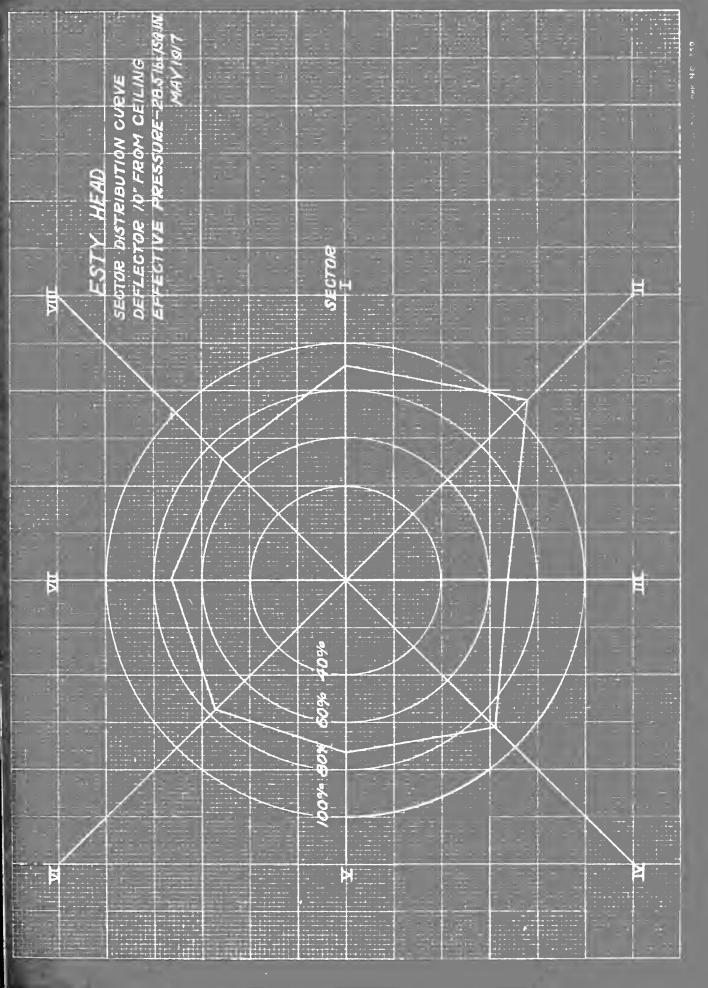
16.23 13.3 14.1

% in Sector 90.8 107.7 67.3

72.8 72.8 88.8 72.8 77.

20 ESTY HEAD ZONE DISTRIBUTION CURVE DETLECTIVE PRESSURE—RELING ANY JOIT 10 GALLING SOME—DISTRIBUTION CURVE ANY JOIT ANY JOINT ANY JOIN				
BILITY				1
BILLY BILLY				CURVE
BULLY BULLY	۵			MAY!
BILLIP ALLIP A				
BILLYN BLILYN BLILY BLILYN BLILY BLILYN BLILYN BLILYN BLILYN BLILYN BLILYN BLILYN				
BILLING SOME FROM CENTER-FEET	WIK.			
BILLING SONE FROM CENTER-FEET	(114.6)			
BILLY BILLY ZONE-DISTANCE FROM CENTER-FEET	s / sw			
BILLY BILLY ZONE - DISTANCE FROM CENTER-FEET	o truvo			
BILITY BARGE FROM CENTER-FEET				
ZONE-DISTANCE FROM CENTER-FEET				
	4	- DISTANCE FR	M CENTER-FEET	9

- ×	
	•



ESTY HEAD

GAUGE PRESSURE, 50 lbs. sq. in; DEFLECTOR 10" FROM CELLING; EFFECTIVE PRESSURE, 55.5 lbs. sq. in. runs.

pe .	Zone	13.32	14.62	16.61	11.68	62.6	9.86	
Gals.	· пты • о.д • Бе	.0848	.1714	. 2380	.2152	. 2422	.3176	
Gals.	епот пт	26.97	89.68	33.64	23.66	19.02	19.95	
Weight	Zone	A-224.75	B-246.8	°-280.35	D-197.2	E-158.5	F-166.25	
Total	nergue.	54.25 46.50 61.00 63.00	106.8 140.0	138.75 141.6	107.7	158.5	166.25	
	VIII	12.00 12.75 12.25 13.25	21.60 25.75	26.50	19.40	30.50	15.00	
	VII	7.50 1.75 1.25 2.25	16.10	15.50	18.40 6.75	26.00	30.00	
	VI	2.00 3.75 7.75 5.25	7.60 18.75	11.50	10.40	17.50	18.00	
0 R S	Λ	4.25 7.25 11.75	16.10 26.25	16.75	14.40 11.75	15.00	24.25	
田田	IV	13.0 15.75 17.75 17.25	24.60 30.25	28.00 16.20	12.40 10.25	13.50	16.00	
cos	III	14.0 1.75 0.25 0.25	15.6	26.50	12.90	24.00	26.00	
	II	0.5 1.75 3.75 1.75	2.60	8.00	11.90	17.50	22.00	
	н	1.0 1.75 6.25 12.25	25.85	6.00	7.90	14.50	15.00	
	PANS	чыка	ပ သ	8	9	11	12	

Total Pounds 117.45 111.45 137.95 214.95 178.70 147.95 138.45 226.95

75.48

Total Gallons 14.09 13.37 16.55 25.79 21.46 17.75 16.61 27.25

40.5 Gals. QSector5.0625 5.0625 5.0625 5.0625 5.0625 5.0625 5.0625 5.0625

65.3 101.8 84.7 70.2 65.7 107.7 52.8 55.7 % in Sector

.

•

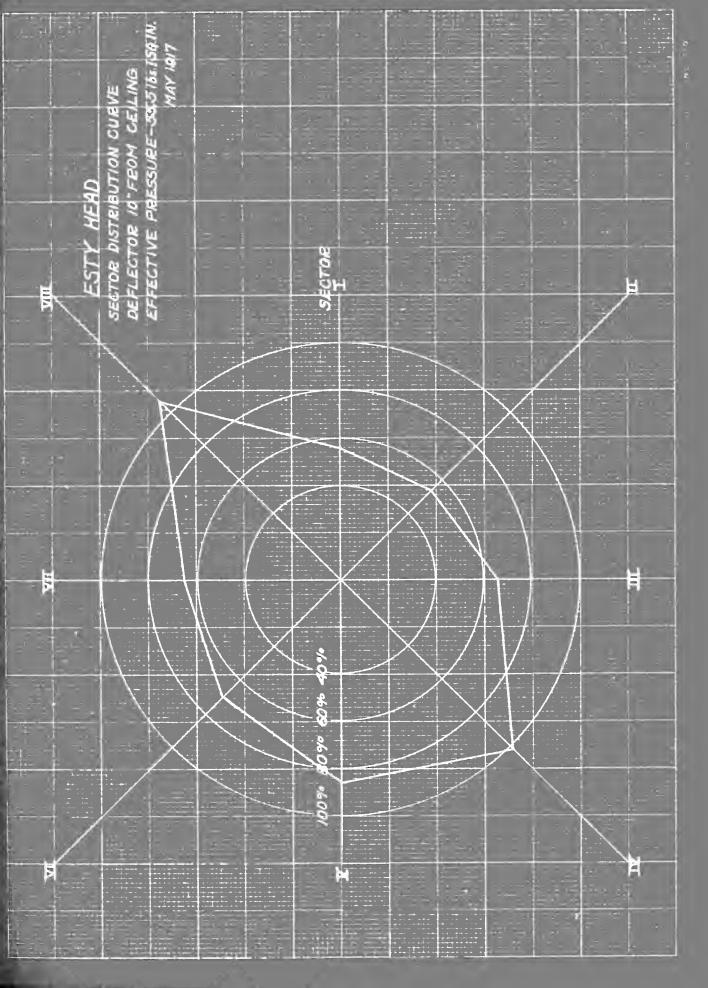
.

•

•

ESTY HEAD	ZANE DISTRIBUTION CURVE DEFLECTOR 10" FROM CEILING EFFECTIVE PRESSURE - 55.515; 15911.					24.52%	C. ON 180
							.FEET 5. 8
							CE FROM CENTER
							ZONE-DISTANC
						75.48 %	
9	, i]	NIWI I	્ર 1 65 / 51√	<i>פעדר</i> 0 9	8	0

•	
	·
•	



HEAD NIAGARA

GAUGE PRESSURE, 5 1bs. sq. in; DEFLECTOR 3" FROM CEILING; EFFECTIVE PRESSURE, 5.75 1bs. sq. in. 5 min. runs.

16 to	Zone	10.15	10.32	11.41	ಜ ಕ	14.0	17.3	72.40	
Gels. So. Ft. Win		.0236	.0431	.0595	.0615	.1315	.2035		
Gals.		٠ ت	7.63	8.41	6.77	10.32	12.75		
Weight	23	A- 62.50	B- 63.55	G- 70.10	D- 56.45	医- 86.00	F-106.25		
Total		20.00 8.00 12.50 22.00	28.55	34.00 36.10	30.45 26.00	86.00	106.25		
	VIII	1.50 .75 .75	5.60	6.50	2.90 3.25	10.00	14.00	52.45	6.29
	VII	3.00 1.75 1.75	3.60	4.00	4.90 3.25	12.50	10.50	55.95	6.71
	IA	3.50 .75 3.75	4.10	3.50	2.90	7.75	9.25	46.95	5.63
의 의	Λ	3.00 1.25 1.25	4.10	4.50 4.70	3.40	00.6	30.00	71.45	8.57
터 이 테	IΛ	1.00 .75 .75	2.85	6.00	2.90	7.00	17.50	50.20	6.02
थ्या	III	2 . 75 . 25 . 25 . 25 . 25 . 25 . 25 . 2	2.25	2.50 3.20	3.15	12.50	09.6	44.20	5.3
	II	3.5 1.25 2.75	4.10	4.50	6.90 4.25	19.50	6.50	59.45	7.13
	н	2.00 3.75 3.75	2.10	2.50	3.25	7.75	00.6	64.20	7.7
	PANS	Hα804	ខ្	8 4	9	11	12	Total Pounds	Total Gallons

14.75 Gals. QSector1.84375 1.84375 1.84375 1.84375 1.84375 1.84375 1.84375 1.84375 1.84375

% in Sector

83.7 77.5 57.6 65.1 93.0 61.25 73.

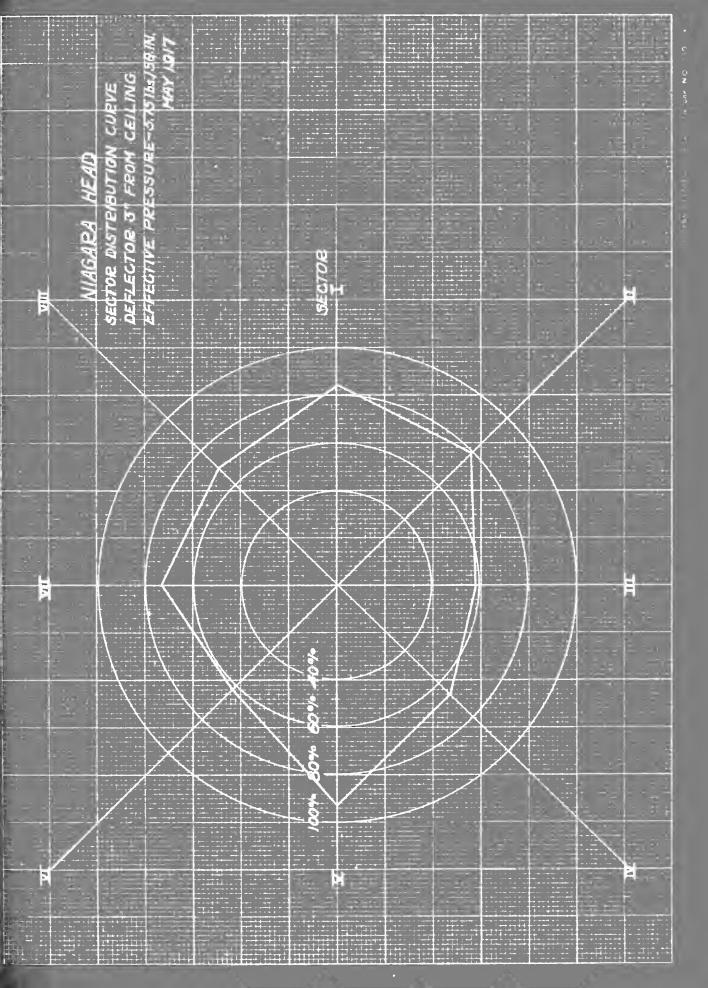
.

. . .

. .

	71/2 27.6%	<i>y</i>) 	n.		0
			OM CENTER-FEET	DISTANCE FR	ZONE	
					72.4%	B
				,		
						פיזדרי פ
						/SIVC
						غ ا <i>ددا</i>
		h				N/M
						20
				6		
1RE-575/bs.159/N. MAY 1917	EFFECTIVE PRESSURE-ST515, 150 IN	3				25
CURVE 4 CEILING	ZONE DISTRIBUTION CURVE DEFLECTOR 3" FROM CEILING	иа				
	MAGAPA HEAD		•			8 €
		Paris			WAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	

	*



NIAGARA HEAD

GAUGE PRESSURE, 25 lbs. sq. in; DEFLECTOR 3" FROM CEILING; EFFECTIVE PRESSURE, 28.0 lbs. sq. in. 5 min. runs.

%÷	Zone	14.7	10.55	12.15	12.10	13.05	7.06	69.61
Gala.		.067	.0887	.1245	.160	.841	.1635	
Gals. In Zone		21.25	15.3	17.6	17.55	18.9	10.25	
Weight	Zone	A-177.00	B-127.30	C-146.60	D-146.20	E-157.50	F- 85.5	
Total Weisht	0	60.50 32.00 30.00 54.50	68.80 F	86.50	69.70 I	157.50 E	85.50 H	85.45
	VIII	12.00 3.75 1.75 2.75	7.60	4.50	3.90 12.75	21.00	7.50	45 8
	VII	6.00 3.75 8.25 8.25	10.10	16.00	7.90 11.75	15.00	2.50	103.95 105.45
	ΙΛ	8.50 2.75 7.25	8.60	11.00	10.40	17.00	4.50	5 103.
0 교	Λ	8.00 3.25 5.75	9.10	13.00	11.40	20.50	39.50	123.9
터 이 ബ	IV	6.00 3.75 1.75	6.10	5.00	3.40 8.75	24.50	16.00	93.95
Ø	III	7.50 2.75 1.75 2.75	9.10	12.00	8.90	21.00	5.50	91.95
	H	5.50 7.75 5.75	11.10	18.00	14.40 12.25	18.00	5.00	130.45
	н	7.00 2.75 7.25 17.75	7.10	7.00	9.40	20.50	2.00	104.95
	PANS	こ の 24	ខេច	8	9	נו	12	Total Pounds

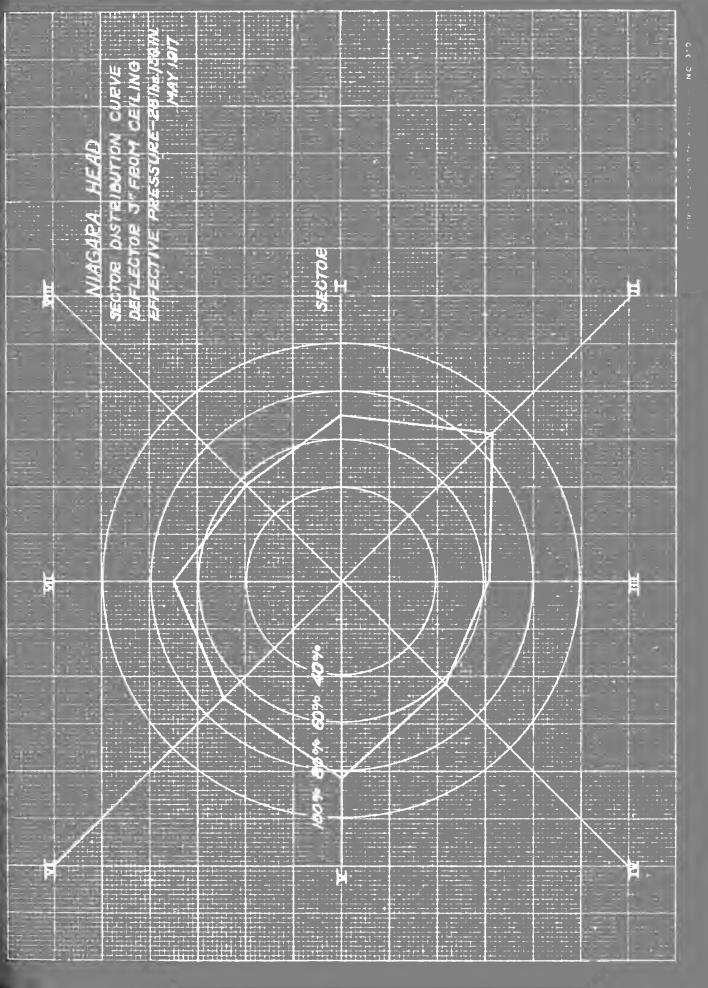
15.65 11.03 11.27 14.87 12.47 12.65 10.25 Gallons 12.6 Total

56.8 70.25 69.8 82.5 61.5 61.0 86.8 70.0 % in Sector

29.0 Gals. QSector 3.625 3.625 3.625 3.625 3.625 3.625 3.625

CURVE	FROM CEILING ESSURE - 28 162 1591N. MAY 1917						c c c
WIAGARA HEAD	DEFLECTOR 3" FROM CEILIN EFFECTIVE PRESSURE - 28						30.39%
Zox	DEF						۲ د
							-FEET
							EOM CENTER-FEET
							ZONE- DISTANCE FE
						%	ZONE
						9, 19.69	· · ·
300	3	8	NIWI	105/5NO Q	9 9	જ	0

•	



	300
	_
	•
•	

NIAGARA HEAD

GAUGE PRESSURE, 50 lbs. sq. in; DEFLECTOR 3" FROM CEILING; EFFECTIVE PRESSURE, 55.75 lbs. sq. in. 5 min. runs.

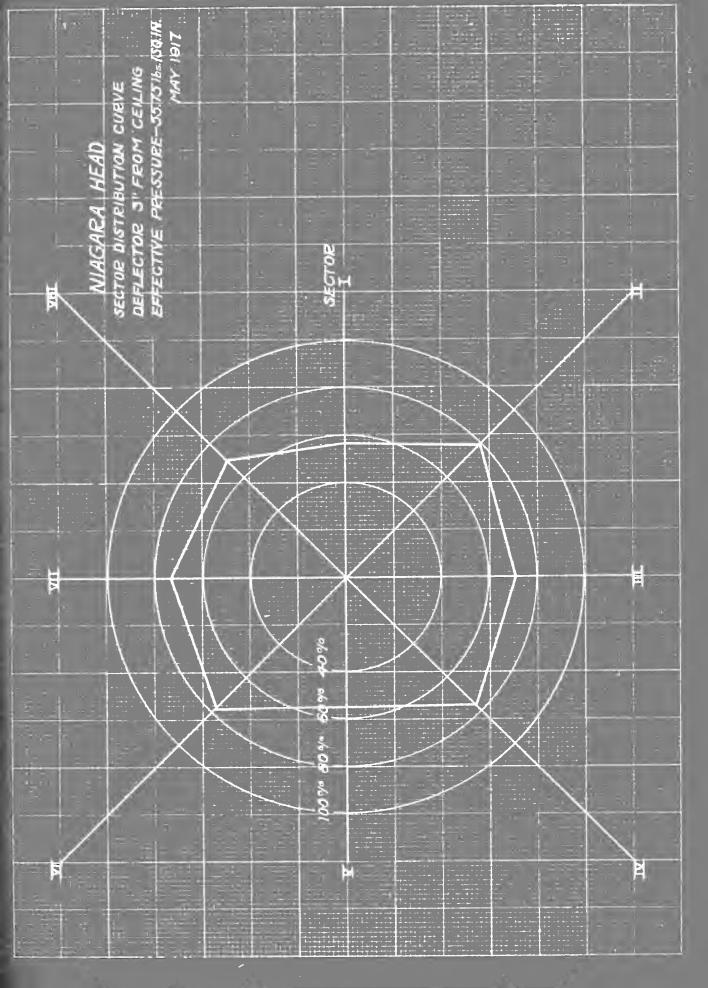
89.4 X	Zone	17.2	12.3	10.35	13.4	10.5	5.95	69.70			
Gala.	• 11 Thr • 2 4 • 5 C	.108	.1425	.146	. 244	. 268	.19				
Gals.		34.4	24.6	20.7	86.8	21.0	11.9				
Weight	Zone	A-286.0	B-202.8	6-172.1	D-222.7	E-175.0	F- 99.5			Gals.	
Total	AG TON	106.0 54.50 35.00 90.50	125.8	79.5	92.2 130.50	175.0	99.5	146.20		40.0	
	VIII	17.5 11.75 4.75 9.25	14.1 9.0	4.5	6.9	24.0	9.0	148.45	17.5	5.0	0.07
	VII	9.5 10.25 4.75 12.25	18.6 11.25	11.0	5.9 18.25	24.0	9.5	163.45]	17.8	5.0	72.2
	ΛI	15.5 4.75 4.75 14.75	16.1 14.25	13.0	14.9 18.75	18.0	11.0	95	19.6	5.0	78.4
이 찌 입	Λ	9.0 3.25 2.75 5.75	13.1 4.25	9.0	11.4	20.5	26.5	20 113	13.7	0.3	54.8
의 의	IV	16.0 7.25 3.75 12.75	13.1	6.5	10.9	28.5	19.0	45 159.20	19.8	5.0	8.94
थ।	III	16.5 3.25 2.25 7.25	20.6 6.25	6.5	12.9 21.75	27.5	11.0	5 145.45	17.5	5.0	70.0
	II	11.5 11.25 6.75 13.25	2 1. 6 12.25	18.5	16.4	11.0	7.0	163.45	19.6	5.0	78.4
	Н	10.5 2.75 5.25 15.25	8.6 9.75	10.5	12.9	21.5	0.9	117.95	14.15	0.3	56.6
	PANS	L 0004	တ သ	8-4	9	11	12	Total Pounds]	Total Gallons	QSector	% in Sector

.

. . .

			NIAGARA HEAD ZONE DISTRIBUTION GURVE DEFLECTOR 3" FROM CEILING EFFECTIVE PRESSURE-557516s (SAIN)
			E LING 675/65/59
			- 1
	Ministration of the last		
	THE RESERVE TO A SECOND PROPERTY OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TO A SECOND PROPERTY OF THE PERSON NAMED IN COLUMN TO A SE		
r b s/:			
os 69.7 %			
ZONE-	- DISTANCE FROM CENTIL	ER-FEET S B 6 A	7/2

	4		
		•	
	-		





HEAD MIAGARA

GAUGE PRESSURE, 5 1bs. sq. in; DEFLECTOR 6" FROM CELLING; EFFECTIVE PRESSURE, 5.75 1bs. sq. in. 5 min. runs.

P6 2	Zone	10.5	10.5	11.85	9.65	11.05	13.8	67.35
Gala.		.0239	.0441	.0605	.0635	.102	.159	
Gals.		7.62	7.63	8.57	66*9	8.01	10.	
Weight	Zone	A63.45	B63.65	C71.40	D58.25	E66.75	F83.25	
Total	9 T S T S II	16.60 9.75 18.60 18.50	24.30	31.50	30.75	66.75	83.25	
	VIII	1.00 0.75 1.25 2.75	4.10	4.50	2.40	11.50	7.50	45.95
	VII	2.10 2.10 2.10 2.00	2.60	2.50	3.10	8.25	6.25	40.50 45.95
	ΙΛ	2.50 0.75 1.25 1.75	3.10 4.25	3.50	2.40	00•9	00.9	38.45
ଥା ଆ ଠା	Λ	2.50 1.75 1.85 1.85	2.60	4.50 4.70	9.00	8.00	27.50	73.30
四回	IV	1.50 0.75 1.75 3.00	3.60	6.50	3.15	6.50	17.50	52.45
थ्य	III	2.00 1.25 1.25 2.75	2.10	2.50	2.25	6.50	5.50	34.45
	II	3.50 1.25 1.75 2.75	3.60	4.50	5.90	14.00	5.00	55.95
	н	1.50 2.00 5.25 2.25	2.60	3.00	2.40	00.9	8.00	65.70
	PANS	H01204	က တ	8	10	11	12	Total Pounds

14.5 Gals. QSector 1.8125 1.8125 1.8125 1.8125 1.8125 1.8125 1.8125 1.8125

6.72 4.13 6.29 8.80 4.62 4.86

Total Gallons 7.88

5.52

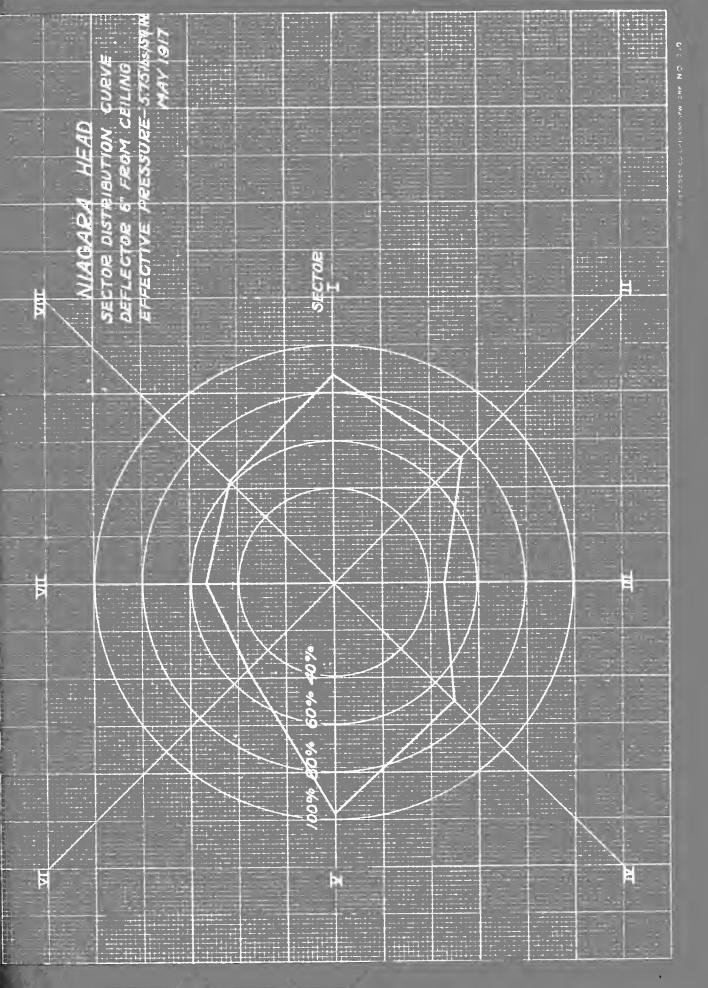
97.0 50.8 53.7 61.0 % in Sector

69.5 87.0 74.2 45.5

.

						1	
85	, fa					NIAG	WIAGARA HEAD
				÷		ZONE DI	ZONE DISTRIBUTION CURVE DEFLECTOR 6" FROM CEILING
×		Fuai		÷		EFFECTIV	EFFECTIVE PRESSURE - 5.75 16. JSQ.IN.
8							
.W.							
בנועי							
bs/sm							
פעדדס פְ				•			
ઝ	67.35%						
0		ZONE-DISTAN	CE FRO	M CENTER-FEET	FEET 6	7	7712065%

		,	
		,	





MIAGARA HEAD

GAUGE PRESSURE, 25 1bs. sq. in; DEFLECTOR 6" FROM CEILING; EFFECTIVE PRESSURE, 28.0 1bs. sq. in. 5 min. runs.

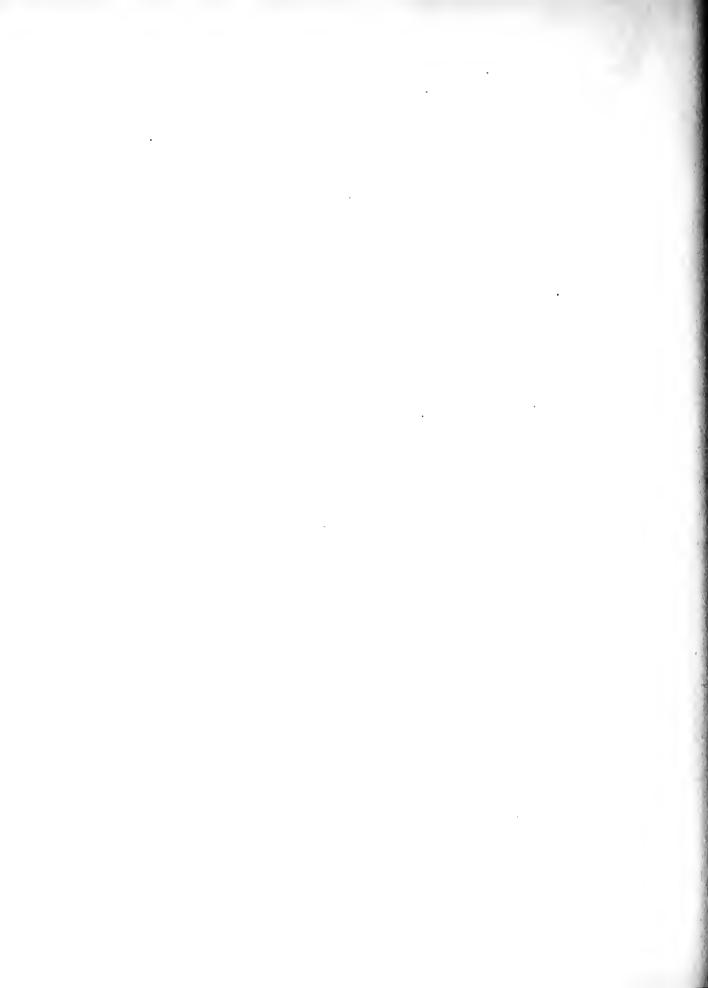
86 i	Zone	15.50	11.90	13.03	10.98	10.35	6.53		68.89
G818.	• HT HE • O 4 • DO	.078	.100	.1335	.145	161.	.151		
Gals.		22.47	17.26	18.90	15.93	15.00	9.48		
Weight	Zone	A-187.25	B-143.80	G-157.60	D-132.70	स-125.00	F- 79.00		
Total	919191	76.25 45.50 26.50 39.00	92.80 51.00	102.00	65. 70	125.00	79.00		45
	VIII	17.50 6.25 2.25 2.25	10.60	6.00	4.40	16.50	00.6		95 92.45
	VII	6.50 6.25 6.25 7.25 7.25 7.25	12.10	17.00	9.40	15.00	5.50		95 99.95
	IA	9.00 7.25 2.75 4.75	12.10	13.00	8.90	13.00	6.50		5 104.95
이 때 의	Λ	10.50 3.75 2.75 1.25	12.60	18.00	11.40	14.50	27.50		112.9
터 이 테	ΔI	13.50 5.75 1.25 1.75	11.10	7.50	4.90	21.50	14.00		98.95
ध्य	III	7.00 4.75 1.75	12.60	15.00	5.90	15.00	00.9		88.45
	II	4.85 8.75 7.25	12.10	17.50	12.40	15.50	5.50		130.70 88
	н	8.00 2.75 5.25 15.25	9.60	8.00	8.40	14.00	5.00		96.95
	PANS	10x 20 4	က တ	8	901	11	12	Total	Pounds

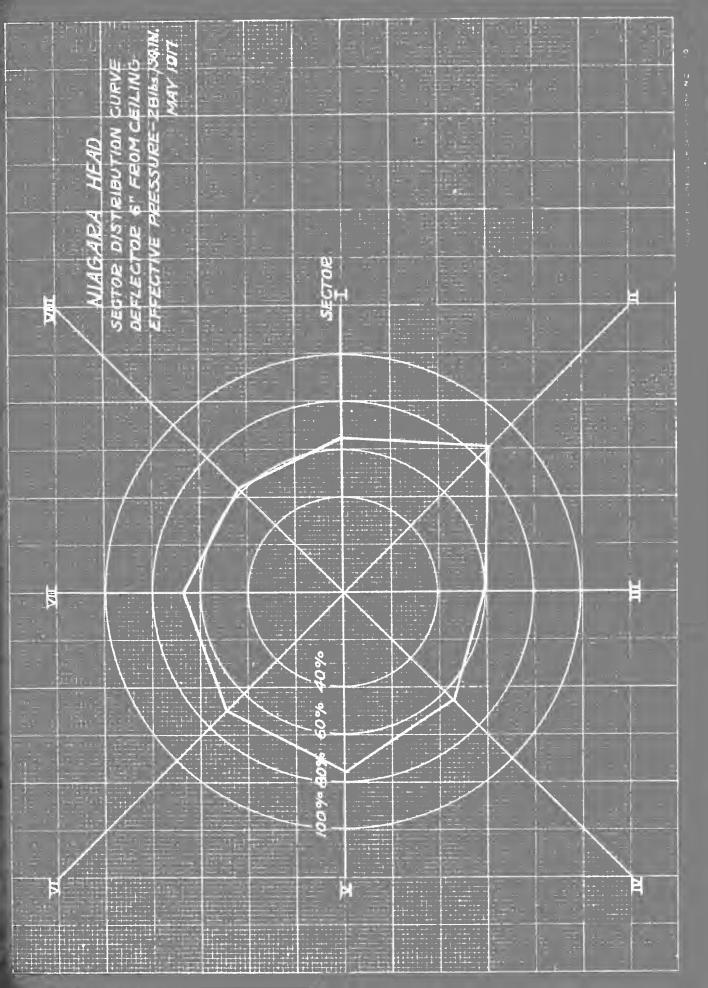
Total Gallons 11.63 15.68 10.6 11.88 13.55 12.6 12.00 11.1

29.0 Gals. QSector 3.625 3.625 3.625 3.625 3.625 3.625 3.625

61.3 % in Sector 64.2 86.5 58.5 65.5 74.7 69.5 66.2

NIAGARA HEAD ZONE DISTRIBUTION CURVE DEFLECTOR 6" FROM CEILING	MAY 1917			
NIAGARA HEAD ZONE DISTRIBUTION CURVE DEFLECTOR 6" FROM CEILING				3/1/1%
				S-FEET B
				ZONE - DISTANCE FROM CENTER-FEET
86	22	S /SCITIMIN.	WOTTV9 O	.05 68.29 %







H E D E H NIAGARA

GAUGE PRESSURE, 50 lbs. sq. in; DEFLECTOR 6" FROM CEILING; EFFECTIVE PRESSURE, 55.75 lbs. sq. in. 5 min. runs.

%;	Zone	16.25	12.35	12.50	11.60	18.65	5.95	67.3	
Gals.		.102	.143	.177	.211	.221	.19		
Gals. In Zone		32.5	24.7	25.0	23.2	17.3	11.9		
Weight	2	A-271.5	B-205.8	9-602-0	D-193.7	E-144.5	F- 99.5		
Total Weight	119-12110	110.5 55.50 42.50 63.00	122.8 83.00	117.5	82.2 111.50	144.5	99.5	146.45	
	VIII	19.5 12.25 8.25 5.25	15.6 9.25	9.5	6.9	18.5	11.0	157.95	17.6
	VII	16.0 10.25 6.25 4.25	16.6 14.75	17.0	8.9	23.5	0.6	157.45	19.0
	VI	15.5 3.75 6.25 13.25	16.1	15.0	12.9	16.0	10.5	45	18.9
ଓ ଆ ଠା	Λ	8.5 2.25 1.75	12.1	11.5	9.9	17.0	28.5	.95 103	12.4
의 의	ΔI	15.5 7.75 3.25 9.25	14.1	11.5	13.9 18.75	20.5	16.0	95 154.	18.6
था	III	14.5 2.75 1.25 3.25	14.1	19.0	7.9	20.5	8.5	117.	14.3
	II	12.5 14.25 9.75	25.6 12.25	23.5 12.2	9.9	9 0	8.0	171.45	20.6
	н	8.5 2.25 5.75 12.75	8.6 11.25	10.5	11.9	19.0	8.0	114.95	13.8
	PANS	このひみ	യ ല	7 8	9	11	12	Total Pounds	Total Gallons

40.0 Gals.

5.0

5.0

5.0

5.0

5.0

5.0

5.0

5.0

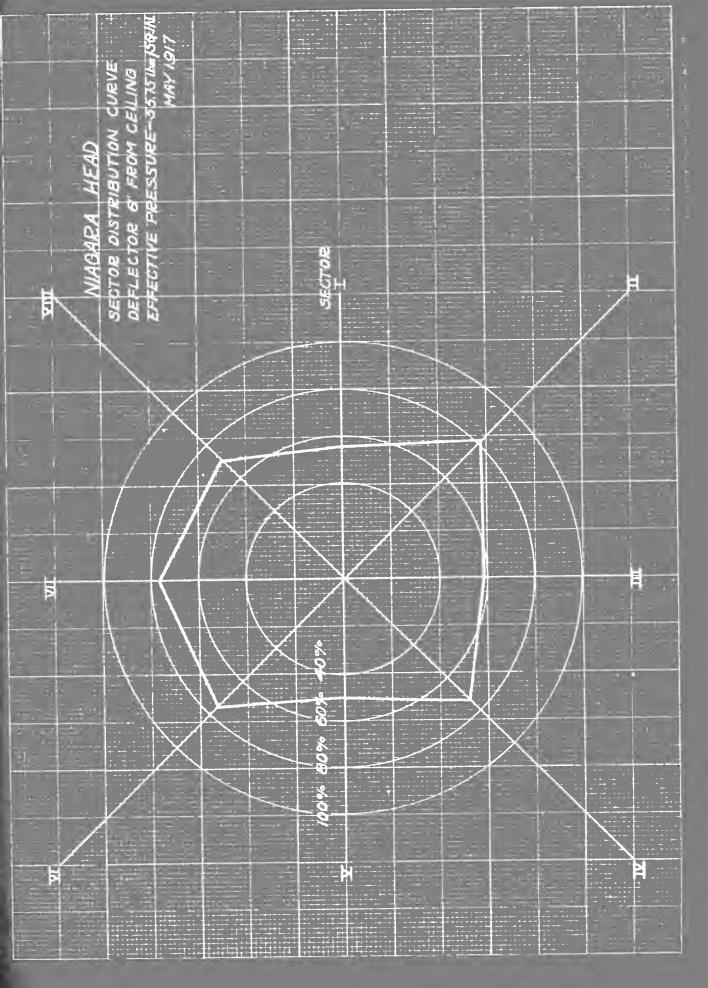
asector

57.2 74.4 49.6 75.6 76.0 78.4

% in Sector 55.2 82.4

ai ai					
ş				NIZGAK	AGARA HEAD
3			E	ZONE DIST	ZONE DISTRIBUTION CURVE DEFLECTOR 6" FROM CEILING
				EFFECTUM	FRESCORE LOS 10 (a)
2					
N/4					
ठ १८/ <i>२</i> ।					
ארד ov					
9 2					
20	67.3%				32.7%
9	L COMP	ZONE - DISTANCE FROM	5	B 6 A 7#	

			. 4
			3
	-		
		•	



		. []

NIAGARA HEAD

GAUGE PRESSURE, 5 lbs. sq. in; DEFLECTOR 10" FROM CEILING; EFFECTIVE PRESSURE, 5.75 lbs. sq. in. 5 min. runs.

P6 +	Zone	10.50	9.93	11.97	7.05	7.53	11.85	58.83
Gals.	• HTW • 0 H • 5C	.024	.0415	.0613	.0464	9690	.137	
Gals.	TIT WOITE	7.65	7.18	8.67	5.10	5.45	8.60	
Weight	Zone	A- 63.75	B- 59.8	G- 72.1	D- 42.7	E- 45.5	F- 71.5	
Total	919191	22.0 11.00 11.50	30.8 29.50	43.0 291	25.7	45.5	71.5	
	VIII	1.0 0.75 0.75 1.75	5.1	0 & 6 &	3.4	9.5	7.0	45.95
	VII	2.55 1.25 2.25	2.6	88 83 80 83	2.9	5 • 5	7.5	34.95
	ΛI	4.0 1.05 0.75 2.25	4.6	4.0	1.9	3.5	3.5	33.45
ଧା ଆ ଓା	Λ	4.5 1.75 1.75	5.1	2 co	3.9	ວ	23.5	61.20
터 이 ബ	IV	1.5 0.75 0.75 1.75	4.6 1.75	13.0 1.2	1.25	4.0	10.0	45,45
था	III	3.0 1.75 1.25	2.85 2.85	20.0	2.4 1.75	4.5	5.0	30.95
	II	13.0 1.75 1.25	3.1	88 89 89	2.9	8	7.5	40.45
	Н	2.5 1.25 3.75	2.60	3.50	3.4	4.50	7.5	62.95
	PANS	ᆸᅈᄶᅀ	က တ	8	01	11	12	Total Pounds

14.5 Gals. QSector1.8125 1.8125 1.8125 1.8125 1.8125 1.8125 1.8125 1.8125

5.5

4.85 3.72 5.45 7.35 4.03 4.18

7.55

rotal Gallons

83.25 53.5 42.0 60.0 81.0 45.5 46.1 60.5 % in Sector

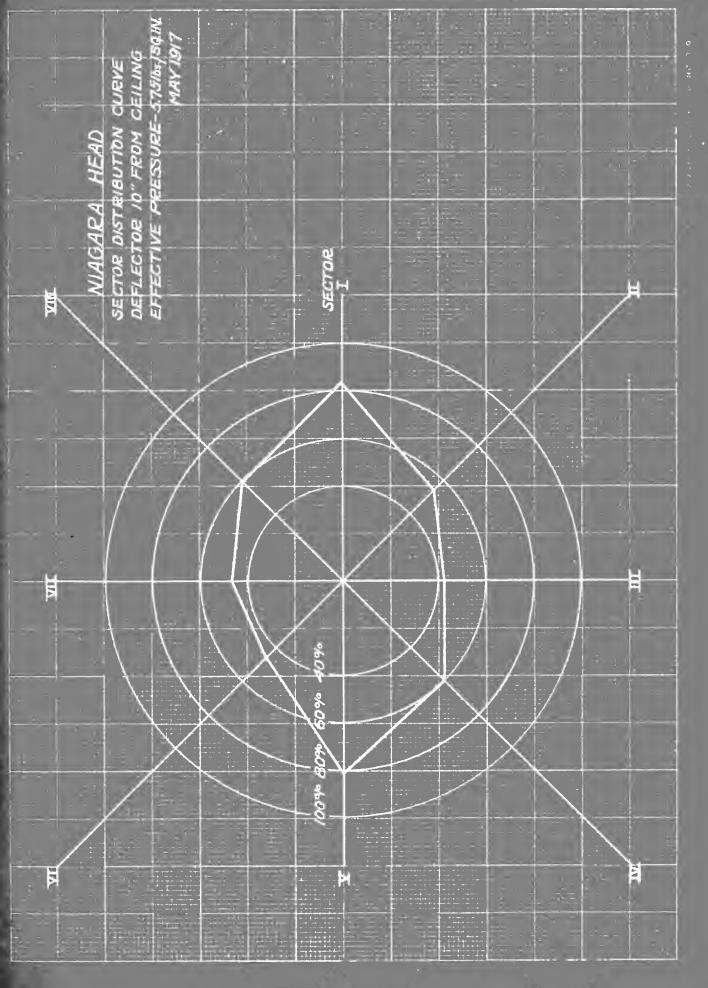
.

.

.

		ZONE	ZONE DISTRIBUTION GURVE
		EFF	EFFECTIVE PRESSURE - 5.75/bs/59/M
Iswornes Q			
58.83%			
Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	ZONE - DISTANCE FROM CENTER - FEET	, o	41.17%

	•		





NIAGARA HEAD

GAUGE PRESSURE, 25 1bs. sq. in; DEFLECTOR 10" FROM CELLING; EFFECTIVE PRESSURE, 28.0 1bs. sq. in. 5 min. runs.

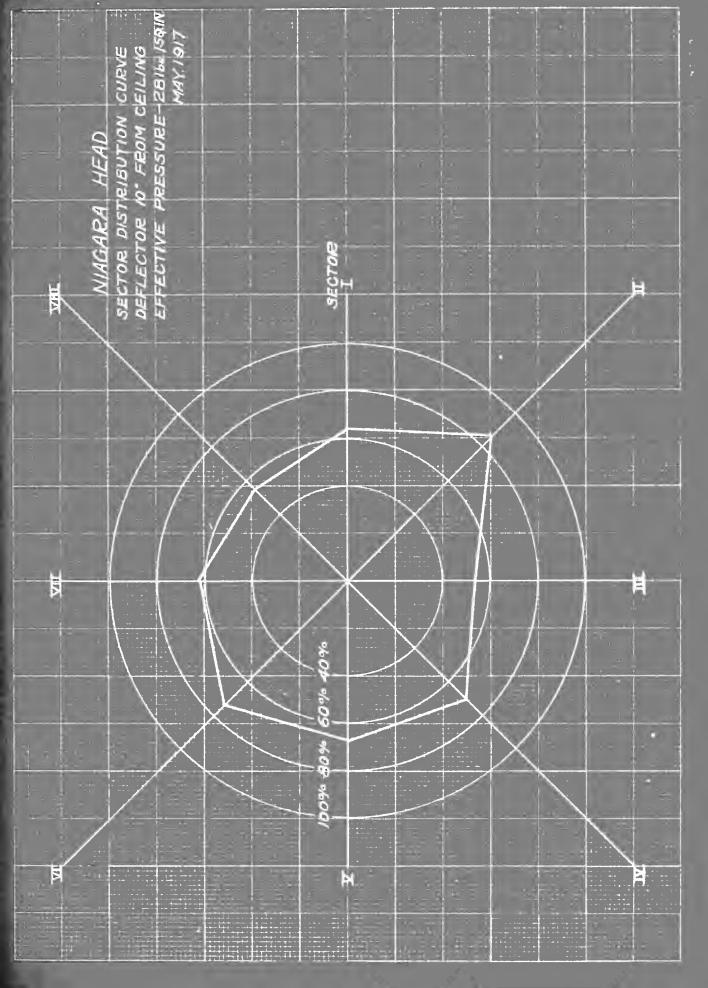
% *	Zone	15.7	11.8	11.95	11.2	7.85	7.45	65.95
Gals. So no Min	•	.0715	660.	.123	.148	.1445	.172	
Gals.		22.68	17.1	17.35	16.27	11.34	10.8	
Weight	Zone	A-189.00	B-142.55	C-144.60	D-135.70	E- 94.5	F- 90.00	
Total	AT ST DIE	71.50 37.50 29.50 50.50	84.80	85.25	67.70	94.50	90.00	77.95
	VIII	13.00 3.75 1.25 2.25	9.10	4.50	3.40	10.50	8.00	92.95 77
	VII	6.00 5.75 3.25 4.25	12.10	12.00	8.90	12.00	7.50	109.95 92
	ÌΛ	9.50 5.75 8.25 8.25	10.60	11.00	9.40	12,50	7.50	95
0 교 의	Λ	8.50 2.75 2.75 1.75	11.10	14.50	9.40	10.00	32.00	5 101.
[의 [의	ÌΙ	15.50 4.25 2.25 4.25	12.60	8.50	6.40	13.00	15.00	96.9 6 129.20 80.95 106.45
Ø	III	7.50 4.25 1.75 2.25	10.10	11.50	8.40	13.50	6.50	80.95
	II	4.50 8.25 8.25 9.75	10.60	16.25 12,45	14.40 11.25	13.00	6.50	129.20
	н	7.00 2.75 6.75 17.75	8.60	7.00	7.40	10.00	7.00	96.98
	PANS		ତ ହ	7 8	9	11	12	Total Pounds

9.85 11.15 12.75 12.20 13.2 6.7 Total Gallons 11.63 15.6 29.0 Gals. 3.625 3.625 3.625 3.625 3.625 QSector 3.625 3.625

53.5 70.5 67.3 73.8 61.5 54.3 % in Sector 64.0 86.

WIAGARA HEAD ZONE DISTRIBUTION CURVE DEFI ECTOR 10" FROM CELLING	EFFECTIVE PRESSURE-Z8 IN. 1917				34.05%	-FEET A 772
8	2	8	12 to 5 / 3	WO 1.16/9	∞ 65.95%	O F ZONE-DISTANCE FROM CENTER-FEET







NIAGARA HEAD

GAUGE PRESSURE, 50 lbs. sq. in; DEFLECTOR 10" FROM CEILING; BFFECTIVE PRESSURE, 55.75 lbs. sq. in.

%i u	Zone	16.8	12.1	12.2	10.3	7.25	6.25	
Gals. Sq.Ft.Min.		.1055	.140	.1725	.187	.185	661.	
Gals. In Zone		33.6	24.2	24.4	20.6	14.5	12.5	
Weight	Zone	A-279.25	B-201.8	G-203.1	D-171.7	E-120.5	F-104.25	
Total Weight		102.0 61.25 45.00	114.3	111.5	83.2	120.5	104.25	
	VIII	18.5 16.0 5.75 4.75	19.1	11.5	6.9	15.5	10.0	
	IIA	14.5 10.25 8.25 14.25	15.6 16.75	15.0	10.4	19.5	9	
	IΛ	11.0 3.75 8.25 12.75	12.1	13.5	11.4	15.5	12,25	
이 제 의	Δ	8.5 2.25 2.75 1.75	11.6	11.0	3.75	11.5	28.0	
의 티	ΙΛ	16.0 7.75 2.75 9.75	14.6	12.0	13.4 15.25	14.5	19.0	
ળા	III	15.0 2.75 1.25 2.25	11.1	15.0	9.9	18.0	9.5	
	II	9.5 16.25 11.25 13.75	21.1	24.0	12.9	12.5	8 •	
	Н	9.0 2.25 4.75 11.75	9.1	8 8 8 8 8 8	9.4	13.5	7.5	
	PANS	H01004	တ ထ	8	9	Ħ	12	

Total Pounds 102.45 172.95 101.45 152.45 96.96 143.20 162.95 148.20

63.90

40.0 Gals. 5.0 17.8 19.5 5.0 17.2 5.0 11.6 5.0 20.8 12.2 18.3 5.0 5.0 5.0 Total Gallons 12.3 5.0 QSector.

73.2 46.4 68.8 78.0 48.8 83.8 59.8 % in Sector

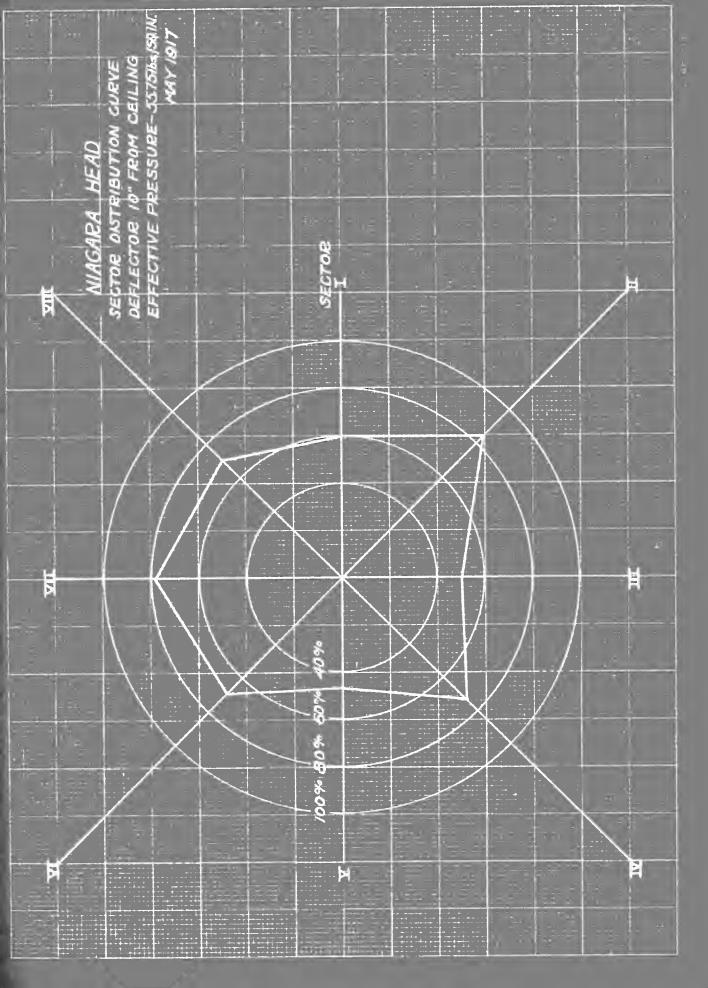
.

. . . .

.

WAGARA HEAD	ZONE DISTRIBUTION CURVE DEFLECTOR IO FFOM GEILING EFFECTIVE PRESSURE - 55.75 Ibs./34IN. MAY 1917				26,7%		7 Tre
							ZONE - DISTANCE FROM CENTER - FEET R P F C S
S.	8	e c	בו: לאווא	(0	V9	.১১ 6.3. 9%	O ZONE-1







MANUFACTURER'S HEAD

GAUGE PRESSURE, 5 1bs. sq. in; DEFLECTOR 3" FROM CEILING; EFFECTIVE PRESSURE, 5.75 1bs. sq. in. 10 min. runs.

%i	Zone	7.6	8.15	13.45	12.8	25.6	28.15	95.75	
Gals. So.Ft.Min.		.0196	620.	.0785	960.	.2685	.369		
Gals. In Zone		12.50	13.45	22.2	21.1	42.2	46.4		
Weight	Zone	A-104.	B-112.	C-185.	D-176.	E-351.	F-386.		
Total Weight	0	23.0 24.0 28.0 28.0	47.6 64.55	94.75 90.55	87.7	351.25	386.0	151.95	
	VIII	8.448 8.33.93 6.63	6.6	10.01	10.9	57.7	24.3		
	VII	44.0 6.0 6.0 6.0 6.0 7.0 7.0	8.35	11.75	9.9	42.5	48.75	204.7 177.45	
	ΙΛ	3.50 2.00 2.75 4.25	6.6 9.25	16.5	22.9	48.0	62.0	45 204	
이 제 의	Λ	.75 1.00 1.50 3.50	4.85	6.00	5.40	16.75	61.50	35 108.	
터 이 ബ	IV	25.54 27.50 27.50 27.50	5.35 9.75	7.75	8.9 14.0	30.0	40.5	144.	
গ্ৰা	III	1.75	3.6	6.0	8.4	25.5	58.7	143.15	
	II	3.5 6.25 2.25 2.25	7.6	31.75 15.95	16.4	75.5	48.5	239.7	
	н	3.7 1.95 1.75 2.25	4.6	5.0	4.9	55.3	41.3	143.25	
	PANS	1 02 D 4	က တ	8	9	11	22	Total Pounds	1

^{18.25} 24.65 21.3 17.4 13.0 17.2 28.8 Total Gallons 17.2

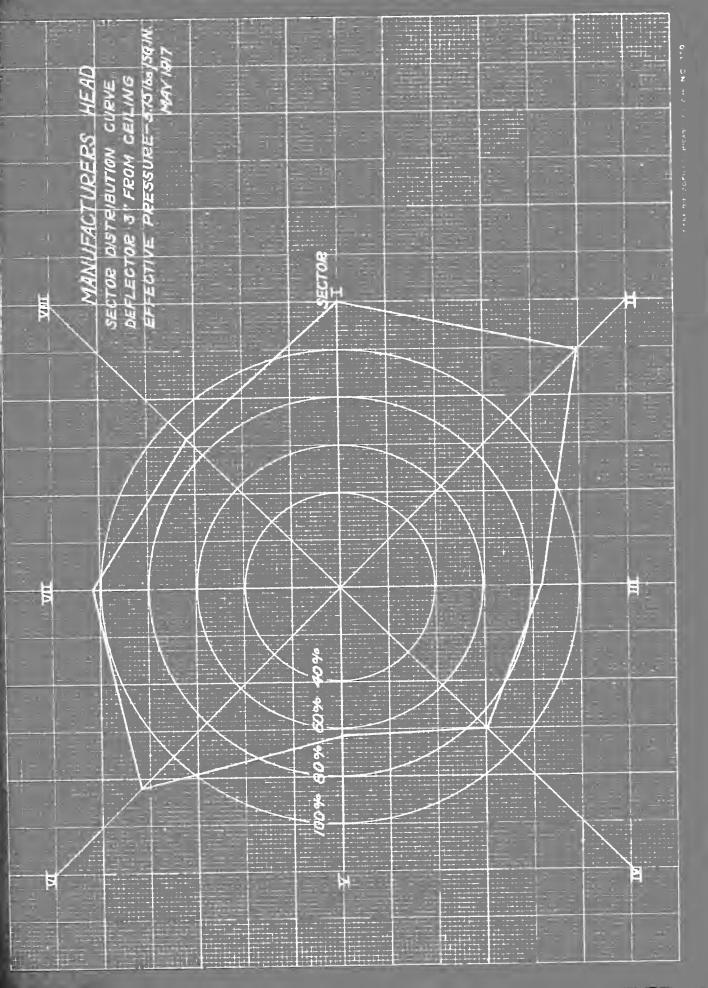
^{16.5} Gals. 2.06 83.5 84.5 63.0 120. 103.5 88.6 2.06 2.06 2.06 2.06 2.06 2.06 % in Sector 83.5 140. 2.06 Sector

.

.

\$.569							MANUFA	MANUFACT URERS HEAD	S HEAD	
							швы	ZONE DISTRIBUTION CURVE DEFLECTOR 3"FROM CEILING EFFECTIVE PRESSURE - 5.7516s / 501N	BUTION C 5"FROM C. PRESSUR	URVE EILING E-S7576 MAY	5 516s / 581N HAY 1917
8			F								
.20							3				
77/										÷	
בנוש שי							Ŧ.			7	
								21/32		***	
פערד סע פַ						7			*1		1
			7 - 7						-		
نهج	95.75%	i	72.0								
o	L.	ZONE-DISTANCE FROM 2	WCE FROM 3	CENTER-FEET	- <i>FEET</i> 5	, 6	~	7.12	423%		







MANUFACTURER S HEAD

GAUGE PRESSURE, 25 lbs. sq. in; DEFLECTOR 3" FROM CEILING; EFFECTIVE PRESSURE, 29.3 lbs. sq. in. 5 min. runs.

in Zone		10.28	9.56	01.11	18.4	27.4	4.75	
gals. Sq.Ft.Min.		.0545	.0925	.1310	. 280	.5845	.127	
gals. In Zone		17.2	16.0	18.55	30.8	45.9	7.95	
Weight in Zone		A-143.25	B-133.5	C-154.55	D-256.95	压-382.37	F- 66.3	
Total Weight		34.3 37.25 38.70 33.0	64.8 68.70	73.0	159.0	382.37	66.3	
SHOEDES	VIII	3.25 4.75 8.5 7.75	7.10	9.5	28.9	0.61	5.5	
	VII	5.4 5.6 5.0 5.0 5.0 5.0 5.0	8.60	0 0 0	24.4 15.25	43.0	4.8	
	VI	3.25 3.25 2.25 2.75	12.1	15.5 10.45	10.9	74.5	5.75	
	Δ	1.25	3.10	4.75	16.15	40.2	23.0	
	ΔI	2.0 4.75 7.75 6.0	5.85	6.25	7.4	30.25	11.5	
	III	4.75 3.50 5.25 5.25	7.35 8.5	0 0 0 0	17.9	62.0	5.75	
	II	10.50 13.75 8.75 4.25	16.85	12.25	25.9 53.25	53.75	4.75	
	H	2.75 2.0 2.75	3.85	6.25	28.40	58.0	5.25	
	PANS	H. 03 KD 44	ତ ପ	7 8	9	11	12	

126.45 225.45 87.7 141.45 101.65 188.70 141.40 162.45 Total Pounds

81.49

33.5 Gals. QSector4.1875 4.1875 4.1875 4.1875 4.1875 4.1875 4.1875 4.1875

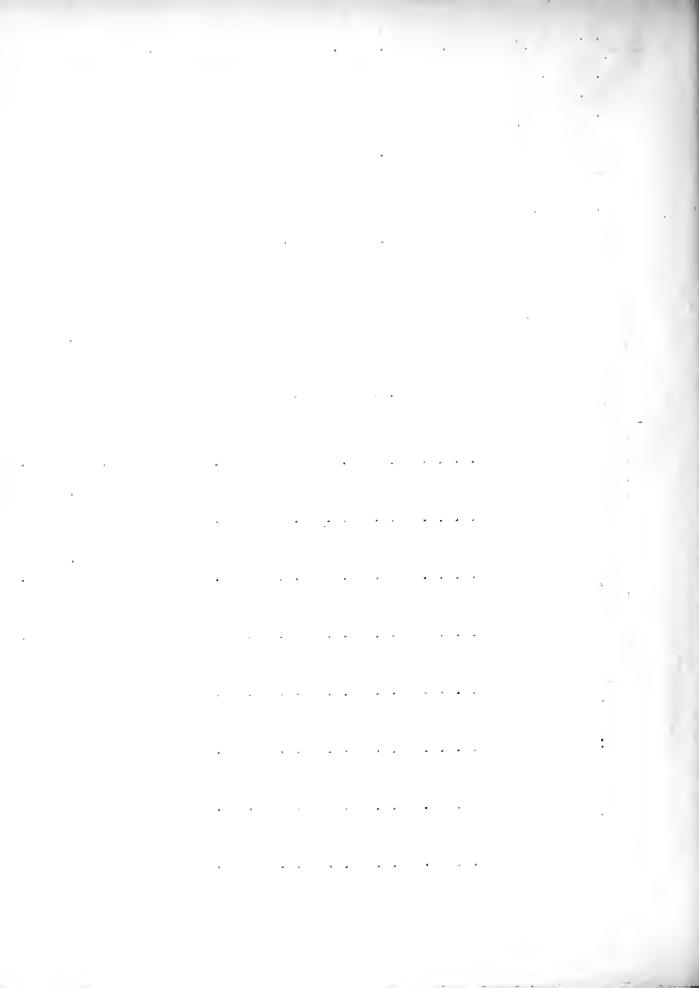
27.05 10.55 17.0 12.2 22.6 17.0 19.5

15.2

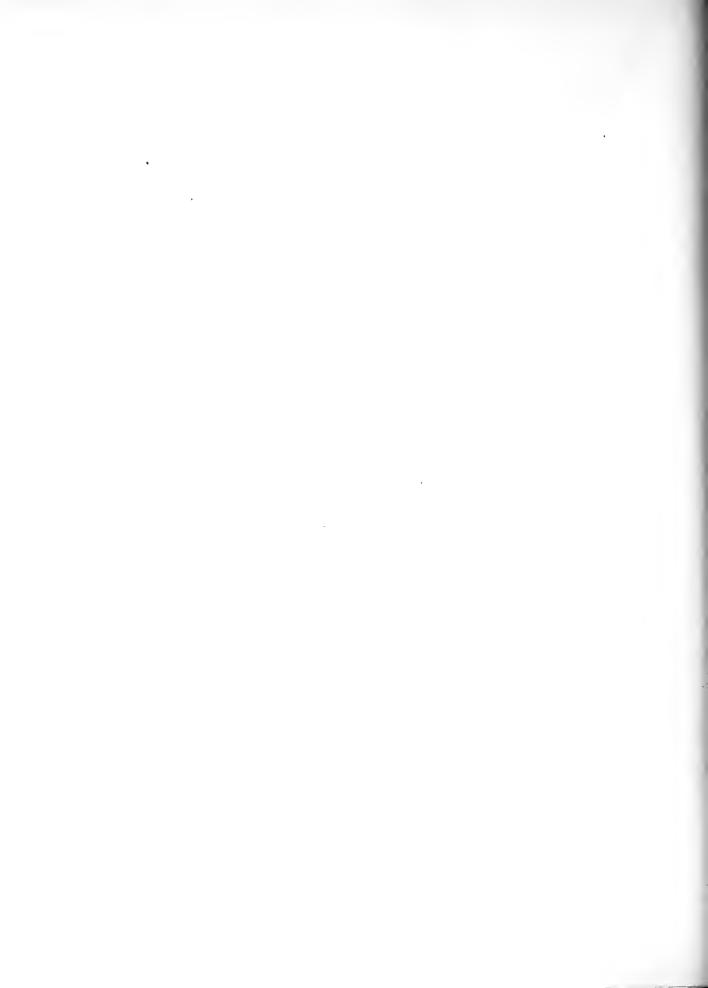
Gallons

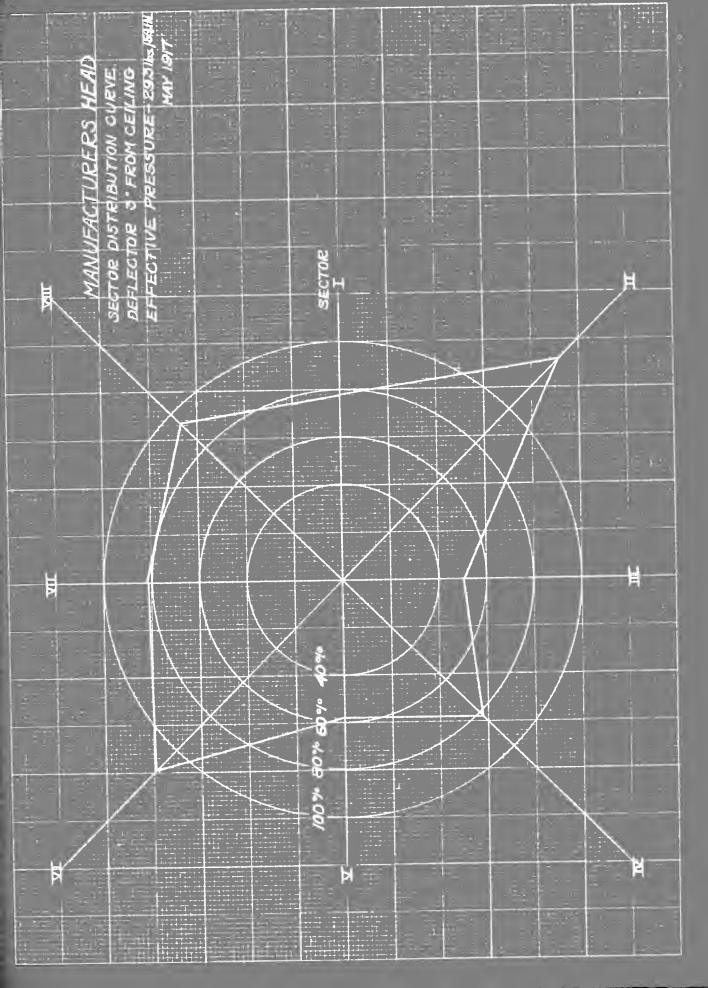
Total

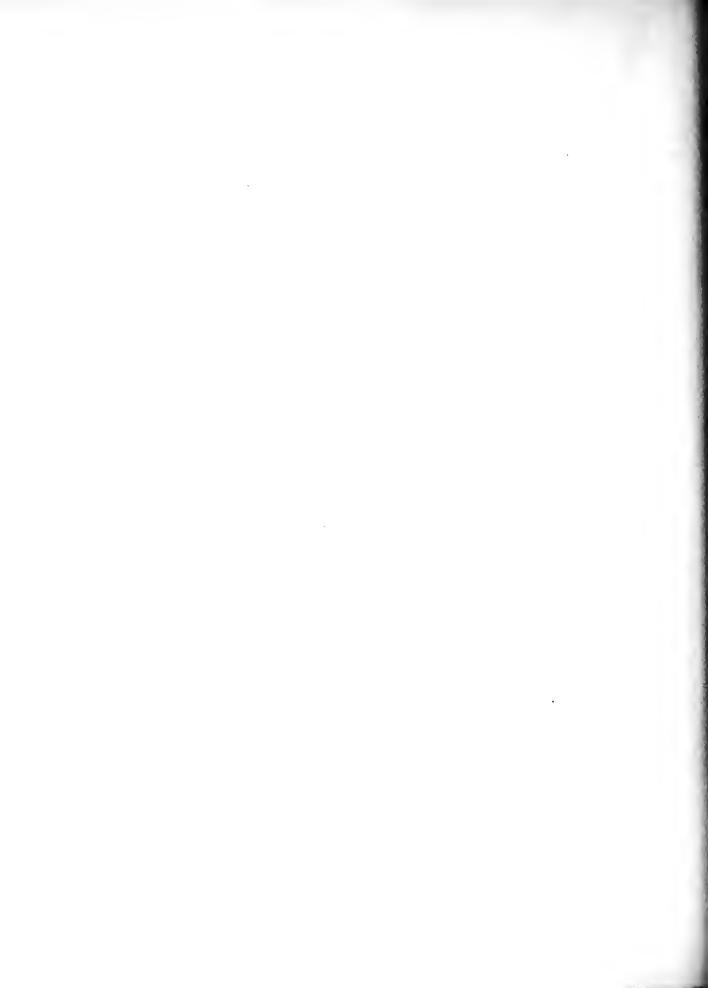
77.6 129.0 50.3 81.2 58.3 112.7 81.3 % in Sector



MANIUFACTURERS HEAD ZONE DISTRIBUTION CURVE DEFLECTOR 3" FROM CEILING	7E PPESSURE - 29.3 Ib				18.5% 6 A TW.
				المراجع والمتحرك المراج	WE FROM CENTER - FEET
.5845		'MW/	G'OS/SMOTIL	, i	ZONE - DISTA







Al H E A വ - 1 (보) 데 데 떠 MANUFAC

GAUGE PRESSURE, 50 lbs. sq. in; DEFLECTOR 3" FROM CEILING; EFFECTIVE PRESSURE, 56.5 lbs. sq. in.

% in Zone		10.1	9.63	15.2	31.2	16.8	4.28	83.21
Gals. Sq.Ft.Min.		.0650	.1165	. 2320	. 584	.439	.140	
Gals. In Zone		20.7	20.1	32.7	64.1	34.4	8.8	
Weight in Zone		A-172.50	B-167.8	6-272.1	D-525-70	E-287.0	F- 73.25	
Total		45.5 43.75 39.26 44.0	85.8	132.0 140.1	261.45 263.75	287.0	73.25	45
	VIII	2.75 5.75 13.25	4.6	8.5	27.9	20.5	6.5	171 03
	VII	8.25 5.25 5.0	14.1 9.25	32.5 14.7	28.9	21.5	7.0	214 15 204 20 171.45
	IA	7.5 7.0 5.25	15.35 10.5	12.5	17.4	59.0	8.25	51 A 1
S H O E S H S H S H S H S H S H S H S H S H S	Δ	2.75 2.25 1.75	3.0	11.0	37.4 4.75	37.0	23.5	ת אצו
	ΙΛ	8 4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	3.85	5.0	13.9	25.0	9.75	7 22 1
	III	8.75 7.5 5.75 6.75	18.6	30.0	48.4	28.5	6.25	000
	H	9.5 13.75 9.75 4.5	19.6	18.0	57.65 68.75	51.5	0.9	200
	H	3.0 1.75 1.75	4.8 6.6	14.5	36.4	44.0	0.9	00 00 E
	PAMS	Чака	က တ	7 8	9	11	12	Total

Pounds 125.2 294.7 236.20 136.7 135.7 214.15 204.20 171.45 Total Gallons 15.05 35.4 41.0 Gals. 5.125 5.125 5.125 5.125 5.125 5.125 QSector5.125 5.125

20.6

24.6

25.8

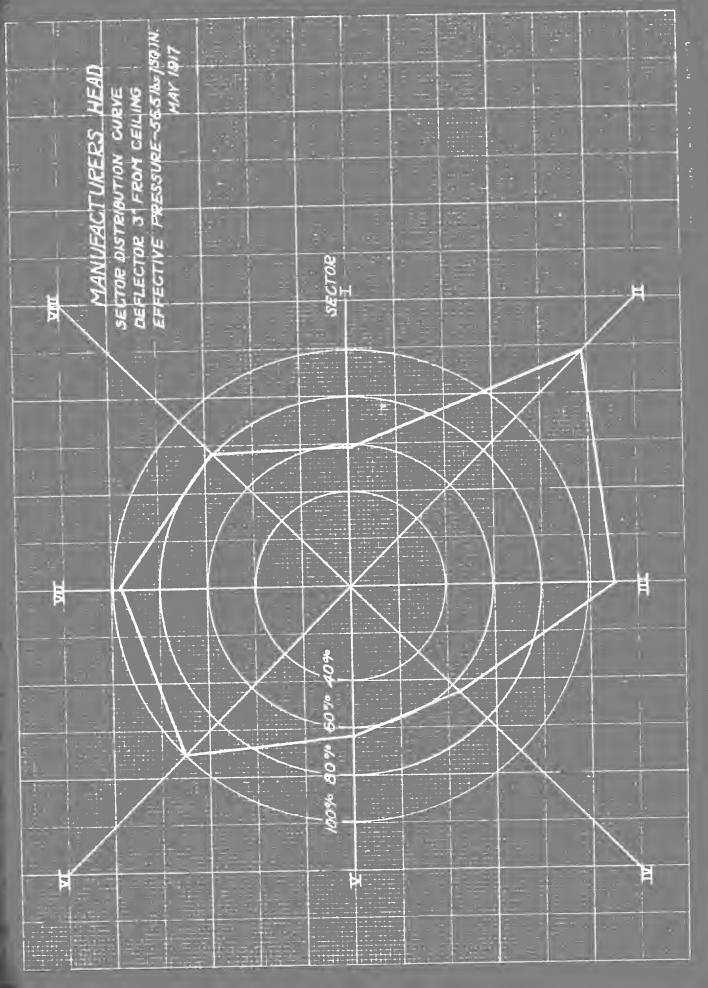
16.4 16.3

28.4

96.0 80.2 58.5 138.0 110.5 64.0 63.5 100.5 % in Sector

		.584			
20		99		MANUFACTURERS HEAD ZONE DISTRIBUTION CURVE DEFLECTOR 3" FROM CEILING	NEAD URVE SEILING
26				EFFECTIVE PRESSURE - 58.0 /bz/>94/A	- 55.5 /bs /59/N. MAY 1917
20					
NIA I					
ठ /sq.FT		•			
SN07					
evi evi					
સ	85.2/%			<i>*62.9/</i>	
0	Z Z Z	ZONE - DISTANCE FROM CI	Y CENTER-FEET	#/2 V	







MANUEACTURER'S HEAD

GAUGE PRESSURE, 5 1bs. sq. in; DEFLECTOR 6" FROM CEILING; EFFECTIVE PRESSURE, 5.75 1bs. sq. in.

16.	2	8.0	8.25	15.15	16.0	28.2	18.5	94.10	
Gels.	· urm·o.a·ñe	.027	.0395	.0885	.12	.296	.243		
Gals.	апоу пт	9.23	9.52	17.5	18.45	32.5	21.3		
Weight	Zone	A- 76.75	B- 79.3	0-145.60	D-153.45	E-270.25	F-177.25		
Total	1181an	19.5 17.0 19.75 20.5	41.05 38.25	72. 75 72.85	75.95	270.25	177.25	116.70	
	VIII	23.75 23.75 25.75	6.1 6.5	8.75	10.4	45.5	8.	109.20 1	
	VII	2.75 3.0 3.75 3.25	5.35	9.95	6.9	28.5	19.5	141.95 10	
	IA	2.75 1.75 2.0 3.75	4.6	12.0	18.9	37.75	26.0	45	
이 임	Δ	2.75	4.1	6.0	6.15	19.5	29.25	55 75.	
의 의	IΛ	1.75 2.75 3.5 2.75	3.6	5.5	6.5	29.0	20.0	.45 106.	
t/2	III	8 8 8 8 9 8 9 8 9 8 9 8 9 9 9 9 9 9 9 9	3.1 6.25	5.5	7.4	24.0	30.5	105	
	II	3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	9.6 10.25	21.5 14.95	13.4	45.25	29.0	165.45	
	Ħ	3.0 1.25 1.25	4.60	6 4 0 3	66.5	40.75	14.5	92.20	
	PANS	H 03 EO 44	ယ္ထ	8	9	11	12	Total Pounds	La+on

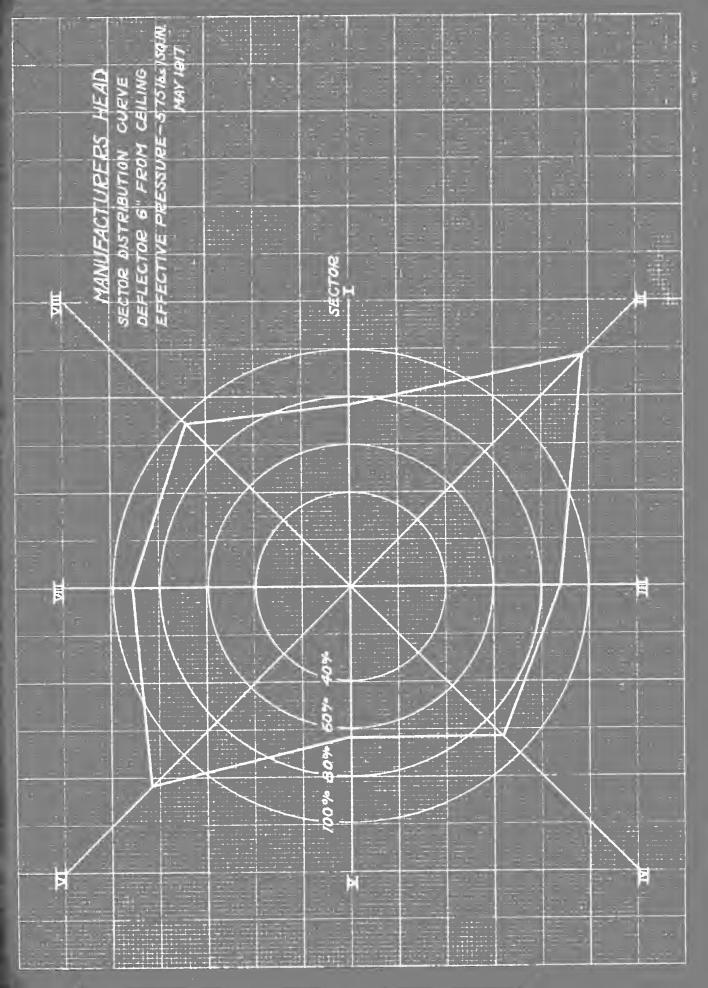
16.5 Gals. 2.06 2.06 9.05 17.0 13.1 2.06 2.06 2.06 12.7 12.8 2.06 2.06 19.9 2.06 11.1 Total Gallons QSector

62.8 118.0 91.0 97.0 88.2 88.8 77.0 138. % in Sector

.

5.75/ba.158/W.				
MANUFACTURERS HEAD ZONE DISTRIBUTION CURVE DEFLECTOR 6" FROM CEILING EFFECTIVE PRESSURE - 5.75/64.159.18				5.9%
Z Ø Ø E				φ γ
				R-FEET
				ZONE + BISTANCE FROM CENTER - FEET
			94.10%	ZONE - DIS
	25 25	 ечггома\ го ?	بع	0







MANUFACTURER'S HEAD

GAUGE PRESSURE, 25 lbs. sq. in; DEFLECTOR 6" FROM CEILING; EFFECTIVE PRESSURE, 29.3 lbs. sq. in. 5 min. runs.

% i	Zone	11.9	11.6	13.7	27.5	21.1	5.0
Gals. Sq.Ft.Min.		.0625	.1125	.1625	.419	.450	.133
Gals. In Zone		19.9	19.4	23.0	46.0	35.3	8.35
Weight	Zone	A-165.50	B-161.3	C-191.35	D-383.2	E-294.0	F- 69.5
Total		39.25 46.75 44.25 35.25	80.8 80.5	95.5 95.85	188.7	294.0	69.5
	VIII.	5.5 11.25 10.25 5.75	14.85 16.5	18.5	28.9	14.0	7.0
	VII	4.5 3.75 3.25 3.0	7.85	9.75	22.9	36.0	7.0
	ΛI	3.0 3.25 4.25 4.75	13.1 9.25	18.5 12.45	13.4	59.0	7.25
0 R S	>	3.75 2.5 1.75	4.85	6.75 3.45	26.65 4.25	33.5	14.25
区 日	IV	2.0 5.75 6.75	7.1 16.5	9.0	11.9	25.75	15.
മ	III	3.75 2.75 5.5 6.75	8.35 10.5	10.5 9.95	18.4 12.75	49.25	6.5
	II	12.75 15.0 9.5 5.25	19.1 10.25	14.25	31.4 50.75	35.25	0.9
	н	8.75 2.0 2.25	5.6 5.75	8 .05 .05	35.15	41.8	6.5
	PANS	10B4	က တ	4	9	11	12

Total Pounds 131.4 222.20 142.95 165.50 104.95 189.70 131.20 176.95

90.8

21.2 22.8 15.8 26.7 17.2 19.9 12.6 Gallons 15.7

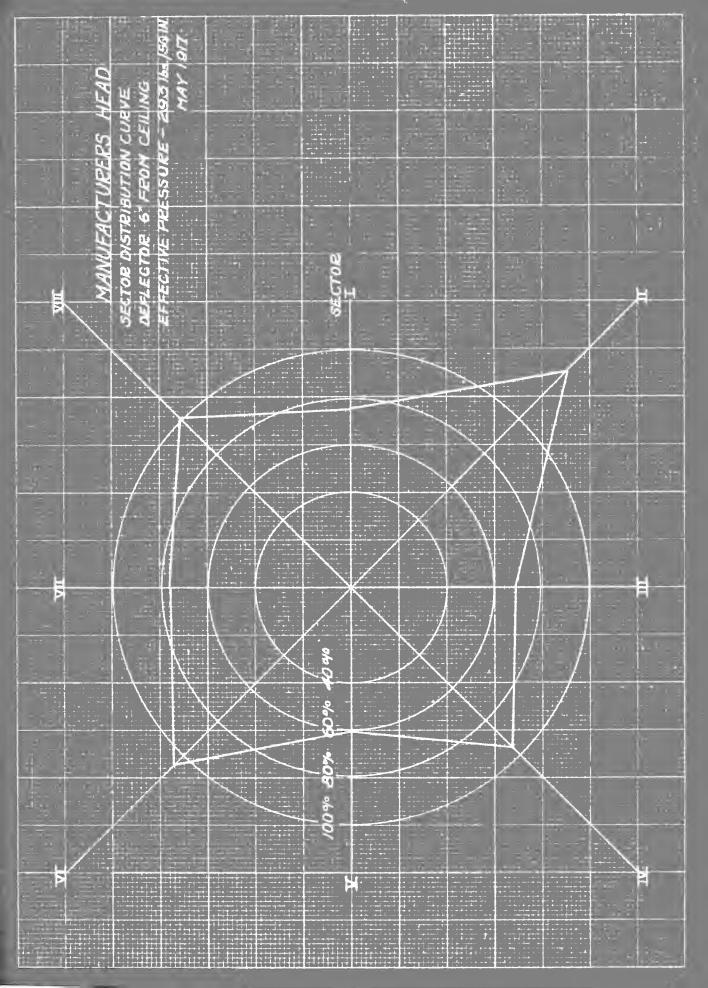
Total

33.5 Gals. QSector4.1875 4.1875 4.1875 4.1875 4.1875 4.1875 4.1875 4.1875

75.5 101.5 75.0 128.0 82.3 95.3 60.4 108. % in Sector

TURERS HEAD TION CURVE FROM CEILING SSURE - 2003 152 / SRIN.					
MANUFACTI NE DISTRIBUT FLECTOR 6 I					7.1%
77					6 P
					ON CENTER-FE
450					- D/S
				%8.06	ZONE
82	52 %	NINI 1 ± 651	פעדר פאצ פ	ઢ	•





H E P MANUFACTURER

GAUGE PRESSURE, 50 lbs. sq. in; DEFLECTOR 6" FROM CEILING; EFFECTIVE PRESSURE, 56.5 lbs. sq. in. 5 min. runs.

i %	2	11.07	11.60	18.10	28.63	12.93	4.88	87.21
Gals. So.Ft.Win.	4	.0715	.1378	.263	. 534	. 338	.161	
Gals. In Zone		25.00	.23.8	37.18	58.7	26.5	10.01	
Weight	Zone	A-189.00	B-198.3	c-309.60	D-489.20	E-221.	F- 83.5	
Total	0	48.25 49.50 45.75 45.50	101.8	158.25 151.35	247.95 241.25	221.0	83.5	190.45
	VIII	3.00 6.25 12.75	9.10	17.00 42.70	27.90 11.75	15.50	7.00	187.95
	VII	9.25 6.75 5.75 5.75	15.60	36.75 14.70	16.90	23.00	8.00	205.70 1
	ΔĬ	6.25 5.25 4.25 25	16.60 11.25	14.75 21.70	16.40	44.25	8.50	8.70 20
이 제 의	Λ	3.00 7.75 .75	4.10	9.25	34.90 4.00	31.00	25.75	11
의 의	ÌΙ	1.00 2.25 4.25 6.75	3.60	5.50	15.90 32.25	22.00	16.00	30 136.45
ωl	İII	10.75 10.5 8.5 9.75	24.6 25.25	38. 18.95	39.9 39.25	23.75	7.	256.20
	II	12.25 14.5 8.0	24.6 10.75	26.5	67.4 63.75	26.5	6.25	295.70
	н	12.25 1.25 0.5 1.0	3.6 2.55	10.5	28.65	18.5	5.0	82.90
	PANS	प ळ छ क	ତ ଯ	7 8	901	11	12	Total Pounds

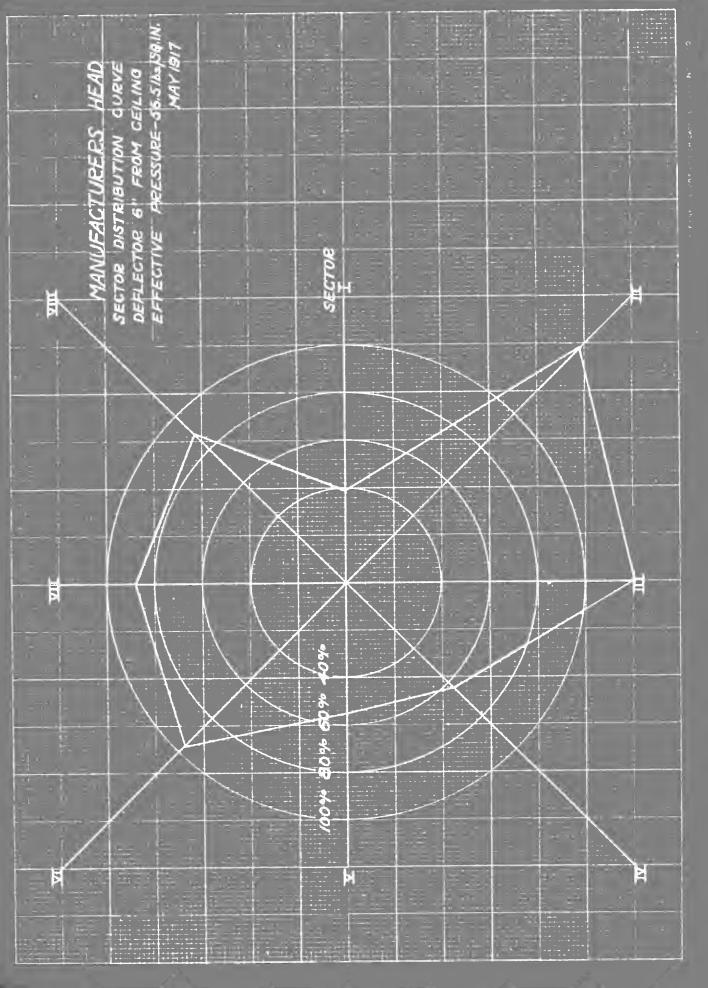
22.58 22.85 16.38 14.23 24.7 Total Gallons 9.97 35.45 30.8

41. Gals. 5.125 5.125 5.125 5.125 5.125 55.6 96.5 88. % in Sector 38.8 138.2 120.2 64. @Sector5.125 5.125 5.125

. . . .

MANUFACTURERS HEAD ZONE DISTRIBUTION CURVE DEFLECTOR 6" FROM CELLING	EFFECTIVE PRESSURE-365/Au/59/7			12.79%	# 12 m
234	1				NCE FROM CENTER-FEE
		NIW (13 OS	-	.os 87.21%	ZONE-DISTA

	•		
•			





AI UI 回 | |出 ଓଧୀ - | ଜ୍ୟା 岡 H 미 티 이 E P A III 国

GAUGE PRESSURE, 5 1bs. sq. in; DEFLECTOR 10" PROM CEILING; EFFECTIVE PRESSURE, 5.75 1bs. sq. in.

i %	Zone	ब्द ८ ८	9.26	15.00	17.30	27.80	13.60	91.18
Gals.	, , , , , , , , , , , , , , , , , , ,	.0213	.0442	.0877	.13	. 292	.178	
Gals. In Zone		9.48	10.69	17.34	19.99	32.04	15.68	
Weight	Zone	A- 79.00	B- 89.00	C-144.60	D-166.45	E-267.00	F-130.75	
Total Weicht	0	20.00 17.25 20.75 21.00	41.30 48.00	72.25	81.95 84.50	267.00	130.75	103.70
	VIII	23.50 20.00 20.00 20.00	5.60	9.00	12.90 8.25	37.25	8.00	
	VII	33.43 34.43 35.43	5.10	7.50 9.45	6.40	24.00	18.00	70 131.45 101.95
	VI	3.00 1.50 4.00	4.10	9.25	18.90 14.75	36.75	18.50	70 131
의 의 이	Δ	2.75 1.00 0.75 0.75	3.60	5.50	6.65	18.75	22.50	20 66.
티 이 떼	ΙΛ	1.50 2.50 3.50 2.75	3.10	4.75	5.90 13.25	29.25	16.50	70 101.80
গো	III	1.25 1.25 2.00 2.75	2.85 6.75	4.25	6.15	30.00	21.25	102.70
	II	88.50 8.50 4.50 0.00	13.10	26.00 17.20	16.90 16.25	52.50	14.00	183.70
	н	2.50 0.75 1.00 1.25	3.85 2.25	6.00	8.15	38.50	12.00	85.70
	PANS	H & & 4	က္ ဟ	8 4	9	11	18	Total Pounds

romars on to

Qsector2.0625 2.0625 2.0625 2.0625 2.0625 2.0625 2.0625 Total Gallons10.25 22.3 12.33 12.14 8.00 15.77 12.24 12.42

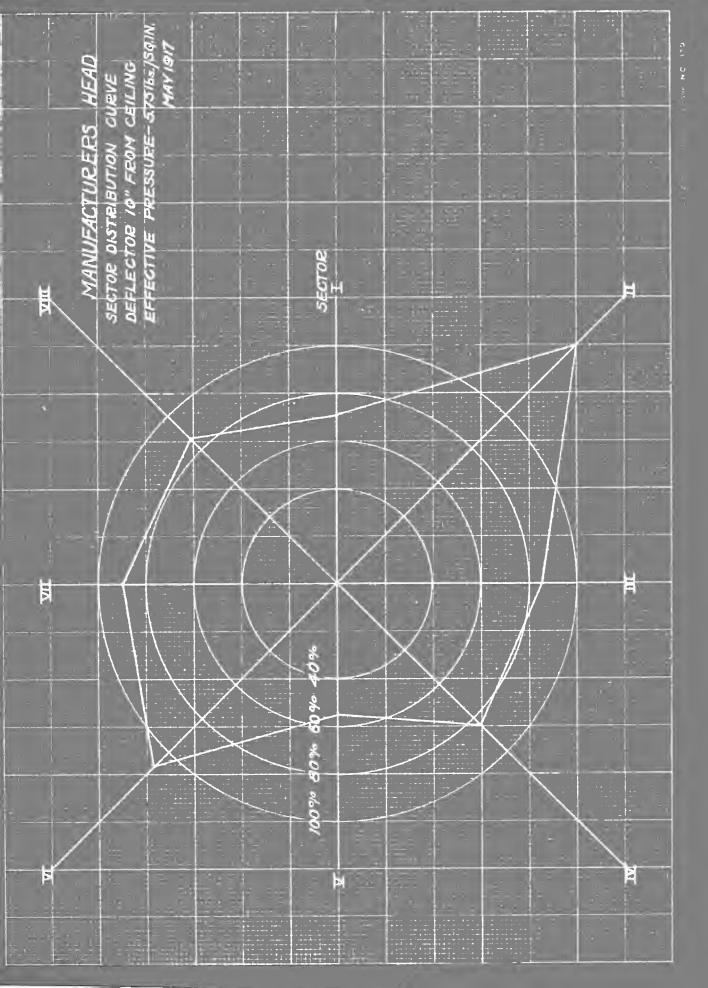
16.5 Gals.

84.2 55.3 109.0 89.8 % in Sector 71.00 140.6 85.4 .

. .

PS HEAD	PRESSURE - 575/6-1997M.					C.C. ON W.C. A.
MANUFACTURERS	VE DISTI LECTOR					882%
	ZON					φ
						CENTER-FEET
						ZONE DISTANCE FROM
					%811/6	ZONE-D
8		28	र्ठ MIM[77 R2\	enittone S	8 OI.R	4

•		
	,	





Al 田田田 MANUFACTURER - S

GAUGE PRESSURE, 25 1bs. sq. in; DEFLECTOR 10" FROM CEILING; EFFECTIVE PRESSURE, 29.3 1bs. sq. in. 5 min. runs.

%in	11.22	12.23	16.95	27.20	15.00	5.51		88.11
Gals. Sq.Ft.Min.	. 059	.119	.201	.414	.319	.147	•	
Gals. In Zone	18.8	20.55	28.4	45.5	25.08	9.24		
Weight in	A-156.50	B-171.30	0-236.60	D-379.20	B-209.25	F- 77.00		
Total Weight	40.50 44.25 38.50	88.05	122.75	187.20	209.25	77.00		73.70
VIII	7.50 13.75 8.25 3.75	19.10	28.50 18.70	19.40	13.75	7.50		124.95 173.70
VII	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	6.60	9.75	23.40	51.75	8.75		
IA	1.50 1.50 3.75 5.75	9.10	19.50	16.40 42.00	40.50	8.75		95 174.70
이 제 이	5.50 2.25 0.75 0.50	6.60	8.50	25.90	23.00	15.75		95 96.
티	2.00 4.75 9.00 7.00	7.60	11.50	15.15	20.75	17.50		167.
Øl H	3.00 1.75 2.75 5.75	8.35	16.50	29.1 5 15.75	34.00	7.25		147.20
II	12.00 14.25 10.25 6.75	22.85 14.25	19.00	30.90 47.75	22.50	5.00		221.95
H	5.50 2.75 1.00	7.85	9.50	26.90 21.25	23.00	6.50		36.611
PANS	100 to 4	ര വ	8	6	11	12	1	rotal Pounds119.

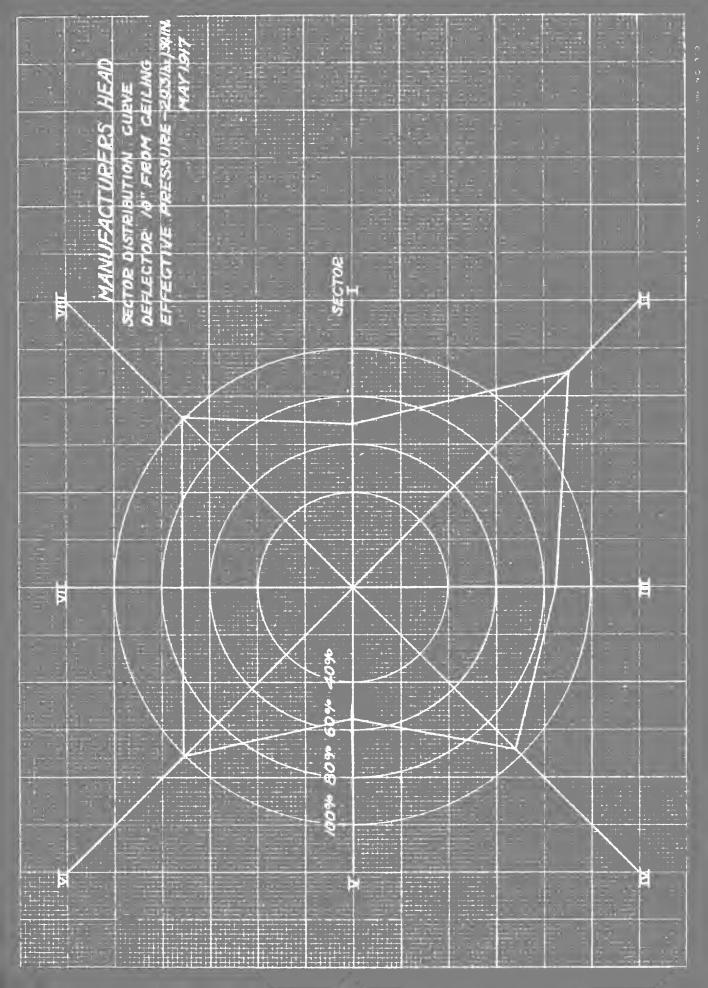
Total Gallons14.4 26.65 17.65 20.18 11.64 20.95 15.00 20.85

33.5 Gals. QSector4.1875 4.1875 4.1875 4.1875 4.1875 4.1875 4.1875 4.1875

55.75 100.00 71.8 99.8 96.5 84.5 127.5 % in Sector 69.

•	II.	ZONE - DISTA	STANCE FROI	POM CEN	M CENTER-FEET	F	7	###	Z 0 2 2 2
6	98.11%							17.89 %	
פערדי פ									
_									
ארד! ארד!איי									
70									
72							DEFLE EFFEC	DEFLECTOR 10" FROM CELLING EFFECTIVE PRESSURE—29312=1391N ANY 1917	LING 1,51b=139/1N. MAY 1917
<u>0</u> 2							MA	MANIJEACTURERS HEAD	EAD
			4/4.	E	-				

4		
-		





Al 41 뙤 田 sol. - । ट्या 国 ۲ ÞΙ 터 ଧ MANUEA

GAUGE PRESSURE, 50 lbs. sq. in; DEFLECTOR 10" FROM CEILING; EFFECTIVE PRESSURE, 56.5 lbs. sq. in. 5 min. runs.

Хоие	11.07	13,65	20.30	24.70	9.84	5.42	84.98
ī.	.0715	.162	.304	.461	. 256	.177	
	22.	28.0	41.6	50.7	20.16	11.1	
Zone	A-189.24	B-223.62	0-346.45	D-422.7	ੜ-167.95	F- 93.45	
	50.70 52.25 39.42 46.87				167.95	93.45	201.95
IIIA	5.50 10.25 7.75				16.00	8.50	77.36
VII	8.55 6.05 6.05 1.6				22.70	9.15	0.45]
VI	4.00 3.75 4.00 5.25	16.35		15.65 37.75	38.00	8.50	3.85 180.45 177.36
Λ	5.40 2.70 0.62 0.21	6.54	14.55 3.05	32.50 6.85	20.00	19.55	
ΙΛ	1.50 3.00 5.00	4.85	8.50	20.90	17.50	21.25	154
III	9.75 9.50 8.25 9.00	28.10		34.90 35.75	18.75	10.25	954
II	12.25 15.25 8.25 4.25	25.10 10.75	31.00 36.20	58.40 48.75	13.50	8.50	34 646
Н	3.25 1.75 1.00	4.35	11.50	22.90 8.25	21.50	7.75	88 70 878 70 854.80 154.80
PANS	प ळ छ स	ତ ଯ	7 8	9	11	18	Total
	ANS I III IV V VI VIII VIII Zone	1 3.25 12.75 9.75 1.50 5.40 4.00 8.55 5.50 50.70 2 1.75 15.25 9.50 3.00 2.70 3.75 6.05 10.25 52.25 A-189.24 22.7 .0715 3 .75 8.25 5.00 0.62 4.00 4.80 7.75 39.42 4 1.00 4.25 9.00 7.75 0.21 5.25 4.16 15.25 46.87	1 3.25 12.75 9.75 1.50 5.40 4.00 8.55 5.50 50.70 1.75 13.25 12.75 9.50 3.00 2.70 3.75 6.05 10.25 52.25 4.189.24 22.7 .0715 3 1.00 4.25 9.00 7.75 0.21 5.25 4.16 15.25 46.87 1.00 4.35 25.10 28.10 4.85 6.54 16.35 15.90 15.10 116.29 B-223.62 28.0 .162 6.25 10.75 26.25 13.75 1.88 11.25 11.45 29.75 107.33 B-223.62 28.0 .162	1 3.25 12.75 9.75 1.50 5.40 4.00 8.55 5.50 50.70 7.75 8.25 8.25 9.50 7.75 0.21 5.25 46.87 1.00 4.25 9.00 7.75 0.21 5.25 4.16 15.25 9.00 7.75 0.21 5.25 4.16 15.25 46.87 1.50 2.75 0.21 5.25 11.45 29.75 10.75 26.25 13.75 1.88 11.25 11.45 29.75 10.73 26.20 187.6 7.25 7.00 18.80 2.70 28.20 3.00 18.45 14.10 32.70 158.85 0.24 4.1.6 3.20 18.80 19.8	1 3.25 12.75 9.75 1.50 5.40 4.00 8.55 5.50 50.70 7.75 8.25 4.00 7.75 6.05 10.25 52.25 4.189.24 22.7 7.75 8.25 8.25 5.00 7.75 0.21 5.25 4.16 15.25 46.87 7.75 8.25 10.75 26.25 13.75 1.88 11.25 11.45 29.75 107.33 8.25 8.20 22.70 8.50 15.90 15.10 116.29 8.22 10.75 26.25 13.75 18.8 11.25 11.45 29.75 107.33 8.22.62 22.70 8.50 18.45 14.10 32.70 158.85 8.25 48.75 35.75 22.00 6.85 37.75 29.80 10.75 199.9 9 22.80 58.40 34.90 20.90 32.50 15.65 13.65 23.90 222.8	3.25 2.75 9.75 1.50 5.40 4.00 8.55 5.50 50.70 5.25	3.25 12.75 9.75 1.50 5.40 4.00 8.55 5.50 50.70 1.50 5.40 4.00 8.55 5.50 50.70 1.50 5.40 4.00 8.55 5.50 50.70 1.50 5.25 5.00 0.62 4.00 4.80 7.75 59.42 4.189.24 22.7 0.715 1.1

Pounds 88.70 272.70 254.20 154.20 113.85 180.45 177.36 201.95

13.65 21.65 20.68 24.2 18.5 Gallons10.65 32.78 30.5 Total

41. Gals. 5.125 5,125 5.125 5.125 5.125 5.125 5.125 QSector5.125

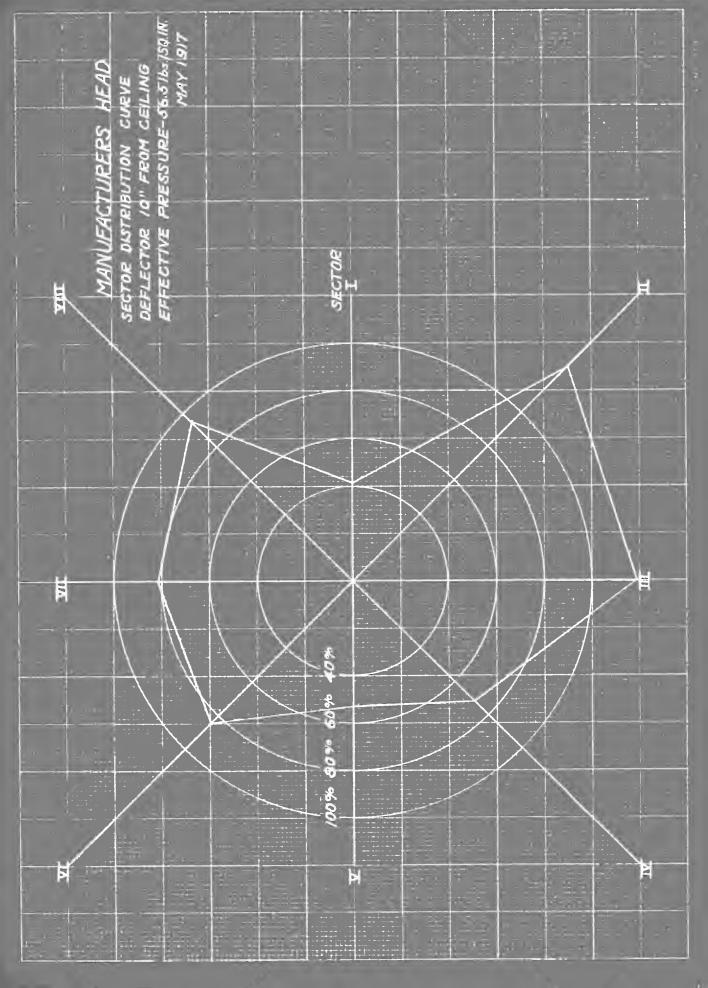
81.

53.3 84.8

72.3 % in Sector 41.5 127.8 119.

SSO WIND TO THE WASTERSON OF THE STRUCK OF T		
ZONE- DISTANCE FROM CENTER-FEET $z \in S$ $z \in $	4	e e
(5.02%)	. 84.98 %	ક્ર
	9טרו פ	
	s/sn	
	N 1.18	
	·N	SZ.
EFFECTIVE PRESSORE SOLVE		3
ZONE DISTRIBUTION CURVE DEFLECTOR 10" FROM CEILING		
MANUFACTUREES HEAD		·
792		







	• *					
			•			
,						
		9				
•						
1 2 3						
. 1						
•						
	4					
		4				
					•	





•			



with the contraction J. Harris 25.06 W 4724

